## Lesson 11 Magnetostatics in Free Space

### Introduction

When a small test charge q travels with velocity  $\vec{u}$  in a magnetic field characterized by a magnetic flux density  $\vec{B}$  (Wb/m<sup>2</sup>), it will experience a magnetic force  $\vec{F}_m = q\vec{u} \times \vec{B}$ . If there is an electric field  $\vec{E}$  as well, the total electromagnetic force is governed by the Lorentz's force equation:

$$\vec{F} = q \left( \vec{E} + \vec{u} \times \vec{B} \right) \tag{11.1}$$

Historically,  $\vec{B}$  is defined by measuring  $\vec{F}_m$  and  $\vec{u}$  experimentally. However, we will start with two fundamental postulates of magnetostatics in free space to define  $\vec{B}$ , from which all experimental laws and the concept of magnetic "potential" can be derived.

## **11.1 Fundamental Postulates**

#### ■ Definition and physical meaning

By Helmholtz's theorem (Lesson 5),  $\vec{B}$  can be uniquely specified if its divergence and curl are given:

$$\nabla \cdot \vec{B} = 0 \tag{11.2}$$

$$\nabla \times \vec{B} = \mu_0 \vec{J} \tag{11.3}$$

where  $\vec{J}$  is the volume current density (A/m<sup>2</sup>), and  $\mu_0$  is the permeability of vacuum. Eq's (11.2), (11.3) indicate that: (1) there is no "flow source" of magnetic field, (2)  $\vec{J}$  acts as the "vortex source" of magnetic field, respectively.

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### Integral forms

By integrating both sides of eq (11.2) over a volume enclosed by surface *S* and applying the divergence theorem [eq. (5.24)], we derive:

$$\oint_{S} \vec{B} \cdot d\vec{s} = 0 \tag{11.4}$$

This means that the magnetic flux lines always close upon themselves, and there is no isolated "magnetic pole".

By integrating both sides of eq. (11.3) over a surface bounded by contour C and applying the Stokes' theorem [eq. (5.29)], we derive the Ampère's circuital law:

$$\oint_C \vec{B} \cdot d\vec{l} = \mu_0 I \tag{11.5}$$

As the Gauss's law in electrostatics, eq. (11.5) relates the magnetic source (I) and field  $\overline{B}$ .

## 11.2 Ampère's Circuital Law

#### ■ Definition and applications

If the current distribution has certain symmetry, such that the tangential component of  $\overline{B}$  is constant over a contour C, eq. (11.5) becomes convenient in determining  $\overline{B}$ .

Example 11-1: Consider an infinitely long conducting wire with circular cross section of radius b, and carrying a steady current I(A) in the +z direction. Find  $\vec{B}$  inside and outside the conductor.

Ans: By cylindrical symmetry,  $\Rightarrow \vec{B} = \begin{cases} \vec{a}_{\phi} B_{\phi 1}(r), & \text{if } r < b \\ \vec{a}_{\phi} B_{\phi 2}(r), & \text{if } r > b \end{cases}$ . Choose a circle of radius r as

the integral path C (Fig. 11-1a).

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(1) For 
$$r < b$$
:  $\oint_{C_1} \vec{B} \cdot d\vec{l} = 2\pi r B_{\phi 1}(r) = \mu_0 \left(\frac{r}{b}\right)^2 I$ ,  $\Rightarrow B_{\phi 1}(r) = \frac{\mu_0 I}{2\pi b^2} r(\infty r).$ 

(2) For 
$$r > b$$
:  $\oint_{C_2} \vec{B} \cdot d\vec{l} = 2\pi r B_{\phi 2}(r) = \mu_0 I$ ,  $\Rightarrow B_{\phi 2}(r) = \frac{\mu_0 I}{2\pi r} (\propto r^{-1}).$ 

This example shows that a conducting wire creates a "circulating" magnetic field outside the wire itself:



Fig. 11-1. (a) Cross-section of the conducting wire. (b) Magnitude of magnetic flux density (after DKC).

Example 11-2: Consider an infinitely long solenoid with air core, n turns per unit length, and carrying a steady current I. Find  $\vec{B}$  inside the solenoid.

Ans: Since (1) $\vec{B} = 0$  outside the solenoid, (2)  $\vec{B}$  is constant and in axial direction inside the solenoid,  $\Rightarrow$  choose a rectangular contour *C* (Fig. 11-2).  $\oint_C \vec{B} \cdot d\vec{l} = BL = \mu_0 (nL)I$ ,  $\Rightarrow$ 



Fig. 11-2. A current-carrying solenoid (after DKC).

## **11.3 Vector Magnetic Potential**

#### ■ Definition and physical meaning

From the null identity of eq. (5.35) and the fundamental postulate of eq. (11.2), magnetic flux density  $\vec{B}$  is divergence-free and can be expressed as the curl of some vector potential field:

$$\vec{B} = \nabla \times \vec{A} \tag{11.8}$$

The flux  $\Phi$  of  $\overline{B}$  over a given area S bounded by contour C is:

$$\Phi(\mathbf{W}\mathbf{b}) = \int_{S} \vec{B} \cdot d\vec{s} = \int_{S} (\nabla \times \vec{A}) \cdot d\vec{s} = \oint_{C} \vec{A} \cdot d\vec{l} .$$

The line integral of  $\vec{A}$  over a contour *C* equals the total magnetic flux passing through the area bounded by *C* (physical meaning of  $\vec{A}$ ).

Unlike scalar electric potential V, we need to specify the divergence of  $\overline{A}$  (in addition to the curl of  $\overline{A}$ , specified by eq. (11.8)) to uniquely define the vector magnetic potential  $\overline{A}$ . In magnetostatics, we choose the Coulomb's gauge:

$$\nabla \cdot \vec{A} = 0 \tag{11.9}$$

Substitute eq's (11.3), (11.8), (11.9) into the definition of vector Laplacian eq. (5.31):

$$abla^2 \vec{A} \equiv \nabla \left( \nabla \cdot \vec{A} \right) - \nabla \times \nabla \times \vec{A} = 0 - \nabla \times \vec{B} = -\mu_0 \vec{J} ,$$

i.e., the vector magnetic potential  $\vec{A}$  is satisfied with a vector Poisson's equation:

$$\nabla^2 \vec{A} = -\mu_0 \vec{J} \tag{11.10}$$

#### <Comment>

Coulomb's gauge is chosen to simplify eq. (11.10). We will choose different gauges in time-varying fields (Lesson 15).

#### Evaluation

Eq. (11.10) can be solved by the following procedures:

(1) By eq. (5.33), eq. (11.10) is equivalent to three scalar Poisson's equations:

$$\nabla^2 A_i = -\mu_0 J_i \ (i = x, y, z)$$

in Cartesian coordinates.

(2) The solution to the scalar Poisson's equation  $\nabla^2 V = -\frac{\rho_v}{\varepsilon_0}$  [eq. (8.1)] is:

$$V(\vec{r}) = \frac{1}{4\pi\varepsilon_0} \int_{V'} \frac{\rho_v(\vec{r}')}{R(\vec{r},\vec{r}')} dv' \quad [\text{eq. (6.15)}].$$

(3) By analogy, the solution to the scalar Poisson's equation  $\nabla^2 A_i = -\mu_0 J_i$  is:

$$A_{i}(\vec{r}) = \frac{\mu_{0}}{4\pi} \int_{V'} \frac{J_{i}(\vec{r}')}{R(\vec{r},\vec{r}')} dv'.$$

(4) Combining x-, y-, z-components,  $\Rightarrow$ 

$$\bar{A}(\bar{r}) = \frac{\mu_0}{4\pi} \int_{V'} \frac{\bar{J}(\bar{r}')}{R(\bar{r},\bar{r}')} dv' \quad (Wb/m)$$
(11.11)

Example 11-3: Find the magnetic potential  $\vec{A}$  and magnetic flux density  $\vec{B}$  in the "bisecting plane z = 0" (not for the entire 3-D space) created by a straight current-carrying wire of length 2L and current I (Fig. 11-3a).

Ans: In cylindrical coordinates, an arbitrary observation point and a source point are located at  $\vec{r} = (r, \phi, 0) = \vec{a}_r r$  ( $\phi = 0 \sim 2\pi$ ), and  $\vec{r}' = (0, \phi, z') = \vec{a}_z z'$  ( $z' = -L \sim L$ ), respectively.  $\Rightarrow$  $R(\vec{r}, \vec{r}') = |\vec{r} - \vec{r}'| = \sqrt{r^2 + {z'}^2}$ ,  $\vec{J}(\vec{r}') = \vec{a}_z \frac{I}{S}$  (S is the cross-sectional area of the wire),

$$dv' = Sdz'. \text{ By eq. (11.11), } \vec{A}(r,\phi,0) = \vec{a}_z \frac{\mu_0 I}{4\pi} \left( \int_{-L}^{L} \frac{dz'}{\sqrt{r^2 + z'^2}} \right) = \vec{a}_z \frac{\mu_0 I}{2\pi} \ln \left[ \frac{1 + \sqrt{1 + (r/L)^2}}{(r/L)} \right].$$

By eq. (11.8), 
$$\vec{B}(r,\phi,0) = \nabla \times (\vec{a}_z A_z) = \vec{a}_r \frac{\partial A_z}{\partial \phi} - \vec{a}_\phi \frac{\partial A_z}{\partial r} = \vec{a}_\phi \frac{\mu_0 I}{2\pi r \sqrt{1 + (r/L)^2}}$$
. Fig. 11-3b

compares the magnetic fields caused by an infinitely wire [dashed, eq. (11.6)] and a finite

wire (solid), respectively.



Fig. 11-3. (a) Geometry of a section of straight wire of length 2L carrying current *I*. (b) Normalized magnitude of magnetic flux density in the bisecting plane.

### <Comment>

1) Since eq. (11.11) is a vector integral, determining  $\vec{B}$  by way of calculating  $\vec{A}$  is less helpful in comparison with determining  $\vec{E}$  by way of calculating scalar potential V.

2) 
$$\bar{B}(r,\phi,0) \rightarrow \bar{a}_{\phi} \frac{\mu_0 I}{2\pi r}$$
 when  $r \ll L$ , consistent with that derived in Example 11-1.

## 11.4 Biot-Savart Law

■ Magnetic field created by current loops

For a closed current loop C' made by thin wire carrying a current I (typical magnetic source), the term  $\vec{J}(\vec{r}')dv'$  in eq. (11.11) becomes  $Id\vec{l}', \Rightarrow$ 

$$\vec{A}(\vec{r}) = \frac{\mu_0 I}{4\pi} \oint_C \frac{d\vec{l}'}{R(\vec{r},\vec{r}')}$$
(11.12)

The resulting magnetic flux density  $\overline{B}$  is governed by Biot-Savart law:

$$\vec{B} = \oint_C d\vec{B}, \ d\vec{B} = \frac{\mu_0 I}{4\pi} \frac{dl' \times \vec{a}_R}{R^2},$$
(11.13)

where  $\vec{a}_R(\vec{r}, \vec{r}') = \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|}$  is the unit vector in the direction from the source point  $\vec{r}'$  to the

observation point  $\vec{r}$ ,  $R(\vec{r},\vec{r}') = |\vec{r} - \vec{r}'|$ ,  $d\vec{B}$  is the magnetic field contributed by a differential current segment.

Proof:

(1) By eq. (11.12), 
$$\vec{B} = \nabla \times \vec{A} = \frac{\mu_0 I}{4\pi} \nabla \times \left[ \oint_C \frac{d\vec{l}'}{R(\vec{r},\vec{r}')} \right] = \frac{\mu_0 I}{4\pi} \oint_C \nabla \times \left[ \frac{d\vec{l}'}{R(\vec{r},\vec{r}')} \right].$$

- (2) By vector identify:  $\nabla \times (R^{-1}d\vec{l}') = R^{-1}(\nabla \times d\vec{l}') + \nabla (R^{-1}) \times d\vec{l}'.$
- (3)  $\nabla \times d\vec{l}' = 0$ , for  $\nabla \times$  is performed with respect to  $\vec{r}$  while  $d\vec{l}'$  only changes with  $\vec{r}'$ (analogous to the fact:  $\frac{d}{dy} f(x) = 0$ ).

(4) 
$$R = \sqrt{\left(x - x'\right)^2 + \left(y - y'\right)^2 + \left(z - z'\right)^2}, \quad \nabla \left(R^{-1}\right) = \vec{a}_x \frac{\partial R^{-1}}{\partial x} + \vec{a}_y \frac{\partial R^{-1}}{\partial y} + \vec{a}_z \frac{\partial R^{-1}}{\partial z} = -\vec{a}_R R^{-2}. \Rightarrow$$

Eq. (11.13) is derived.

### <Comment>

- 1) Eq. (11.13) allows for direct evaluation of  $\vec{B}$  from current distribution without first calculating  $\vec{A}$ . Its counterpart in electrostatics is the Coulomb's law [eq. (6.10)].
- 2) In non-Cartesian coordinates, pay attention to the "position-dependent" unit vectors (e.g.  $\vec{a}_R \neq \vec{a}'_R$ ).

Example 11-4: Find the magnetic flux density  $\vec{B}$  "on the axis" of a circular loop (not for the entire 3-D space) of radius *b* and carrying a current *I* (Fig. 11-4a).

Ans: (1) In cylindrical coordinates, an arbitrary on-axis observation point P and a source point on the loop C' are located at:  $\vec{r} = (0,0,z) = \vec{a}_z z$  and  $\vec{r}' = (b,\phi',0) = \vec{a}'_r b$ , respectively.  $\Rightarrow$  The displacement vector from the source point to the observation point is:  $\vec{r} - \vec{r}' = \vec{a}_R R$ , where  $R = \sqrt{z^2 + b^2}$ ,  $\vec{a}_R = \frac{\vec{a}_z z - \vec{a}'_r b}{R}$ .

(2) The differential displacement of the source point is:  $d\vec{l}' = \vec{a}'_{\phi}bd\phi'$ ,  $\Rightarrow$ 

$$d\vec{l}' \times \vec{a}_R = \left(\vec{a}_{\phi}'bd\phi'\right) \times \frac{\vec{a}_z z - \vec{a}_r'b}{R} = \frac{bd\phi'}{R} \left(\vec{a}_r'z + \vec{a}_zb\right)$$

(3) By eq. (11.13),



Fig. 11-4. (a) A circular loop of radius b carrying current I (after DKC). (b) Normalized magnitude of magnetic flux density on the *z*-axis.

# **11.5 Magnetic Dipole**

A circular current-carrying loop forms a magnetic dipole (Fig. 11-5). The resulting  $\vec{A}$  and  $\vec{B}$  at any position  $\vec{r} = \vec{a}_R R$  (not just on the loop axis) far away from the loop (R >> b) are:

$$\vec{A}(\vec{r}) \approx \frac{\mu_0 \vec{m} \times \vec{a}_R}{4\pi R^2}$$
(11.14)

$$\vec{B}(\vec{r}) \approx \frac{\mu_0 m}{4\pi R^3} \left[ \vec{a}_R 2\cos\theta + \vec{a}_\theta \sin\theta \right]$$
(11.15)

where  $\bar{m} = \bar{a}_z I \pi b^2$  represents the magnetic dipole moment. In general, any current loop forms a magnetic dipole, where the dipole moment  $\bar{m}$  has a magnitude equal to the product of current *I* and loop area *S*, and is in the direction of right thumb as the remaining four fingers follow the direction of current flow:

$$\vec{m} = \vec{a}_m IS \tag{11.16}$$



Fig. 11-5. Evaluation of far-fields generated by a magnetic dipole (after DKC).

<u>Proof</u>: (1) The geometry has  $\phi$  – symmetry in spherical coordinates. It is sufficient to consider an observation point on the *yz*-plane ( $\phi = \pi/2$ ) with position vector:

$$\vec{r} = (R, \theta, \pi/2) = R\vec{a}_R(\theta, \pi/2) = R(\vec{a}_v \sin \theta + \vec{a}_z \cos \theta).$$

An arbitrary source point on the current loop is located at:

$$\bar{r}' = (b, \pi/2, \phi') = b\bar{a}'_R(\pi/2, \phi') = b(\bar{a}_x \cos \phi' + \bar{a}_y \sin \phi'), \quad \phi' = 0 \sim 2\pi.$$

The displacement vector from the source point to the observation point is:

$$\vec{R}_{1} = \vec{r} - \vec{r}' = R\vec{a}_{R}(\theta, \pi/2) - b\vec{a}_{R}'(\pi/2, \phi'), \implies R_{1}^{2} = \vec{R}_{1} \cdot \vec{R}_{1} = R^{2} + b^{2} - 2Rb(\vec{a}_{R} \cdot \vec{a}_{R}'),$$

where  $\vec{a}_R \cdot \vec{a}'_R = \cos \psi = (\vec{a}_y \sin \theta + \vec{a}_z \cos \theta) \cdot (\vec{a}_x \cos \phi' + \vec{a}_y \sin \phi') = \sin \theta \sin \phi', \Rightarrow$ 

$$R_1^{-1} = \left(R^2 + b^2 - 2Rb\sin\theta\sin\phi'\right)^{-1/2} \approx \frac{1}{R} \left(1 + \frac{b}{R}\sin\theta\sin\phi'\right), \text{ given } R \gg b.$$

The differential displacement of the source point is:

$$d\vec{l}' = \vec{a}'_{\phi}bd\phi' = bd\phi' \left(-\vec{a}_x \sin\phi' + \vec{a}_y \cos\phi'\right).$$

(2) By eq. (11.11), 
$$\vec{A}(\vec{r}) = \frac{\mu_0 I}{4\pi} \oint_C \frac{d\vec{l}'}{R_1} \approx \frac{\mu_0 I b}{4\pi R} \oint_C \left(1 + \frac{b}{R} \sin \theta \sin \phi'\right) \left(-\vec{a}_x \sin \phi' + \vec{a}_y \cos \phi'\right) d\phi'$$
  
$$\approx \frac{\mu_0 I b}{4\pi R} \left[-\vec{a}_x \int_0^{2\pi} \left(\sin \phi' + \frac{b}{R} \sin \theta \sin^2 \phi'\right) d\phi' + \vec{a}_y \int_0^{2\pi} \left(\cos \phi' + \frac{b}{R} \sin \theta \sin \phi' \cos \phi'\right) d\phi'\right]$$
$$= \frac{\mu_0 I b}{4\pi R} \left(-\vec{a}_x \frac{b}{R} \sin \theta \cdot \pi\right) = -\vec{a}_x \frac{\mu_0 I \pi b^2 \sin \theta}{4\pi R^2}.$$

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Since  $\vec{m} = \vec{a}_z I \pi b^2$ ,  $\vec{m} \times \vec{a}_R(\theta, \pi/2) = (\vec{a}_z I \pi b^2) \times (\vec{a}_y \sin \theta + \vec{a}_z \cos \theta) = -\vec{a}_x I \pi b^2 \sin \theta$ ,  $\Rightarrow$  $\vec{A}(\vec{r}) = \frac{\mu_0 \vec{m} \times \vec{a}_R}{4\pi R^2},$ 

as predicted by eq. (11.14). For a general observation point 
$$(\phi \neq \pi/2)$$
,  $-\bar{a}_x = \bar{a}_{\phi}(\theta, \pi/2)$  is  
generalized to  $\bar{a}_{\phi}(\theta, \phi)$ ,  $\Rightarrow \bar{A}(\bar{r}) = \bar{a}_{\phi}A_{\phi}$ , where  $A_{\phi}(R, \theta) = \frac{\mu_0 m \sin \theta}{4\pi R^2}$ .  
(3) By eq. (11.8) and the curl formula in spherical coordinates

(3) By eq. (11.8) and the curl formula in spherical coordinates,

$$\bar{B}(\bar{r}) = \nabla \times \left(\bar{a}_{\phi}A_{\phi}\right) \approx \bar{a}_{R} \frac{1}{R\sin\theta} \frac{\partial}{\partial\theta} \left(A_{\phi}\sin\theta\right) - \bar{a}_{\theta} \frac{1}{R} \frac{\partial}{\partial R} \left(A_{\phi}R\right).$$
(i)  $\frac{\partial}{\partial\theta} \left(A_{\phi}\sin\theta\right) = \frac{\mu_{0}m}{4\pi R^{2}} \frac{\partial}{\partial\theta} \left(\sin^{2}\theta\right) = \frac{\mu_{0}m}{4\pi R^{2}} \sin 2\theta$ 
(ii)  $\frac{\partial}{\partial R} \left(A_{\phi}R\right) = \frac{\mu_{0}m\sin\theta}{4\pi} \frac{\partial}{\partial R} \left(\frac{1}{R}\right) = -\frac{\mu_{0}m\sin\theta}{4\pi R^{2}}$ 

$$\Rightarrow \ \bar{B}(\bar{r}) \approx \bar{a}_{R} \frac{1}{R\sin\theta} \frac{\mu_{0}m}{4\pi R^{2}} \sin 2\theta + \bar{a}_{\theta} \frac{1}{R} \frac{\mu_{0}m\sin\theta}{4\pi R^{2}} = \frac{\mu_{0}m}{4\pi R^{3}} \left[\bar{a}_{R}2\cos\theta + \bar{a}_{\theta}\sin\theta\right],$$

as predicted by eq. (11.15).

### <Comment>

Resemblance between eq's (11.14), (6.18) and eq's (11.15), (6.16) implies that the "far-field" patterns established by electric and magnetic dipoles are similar if the electric dipole moment is replaced by the magnetic dipole moment  $(\vec{p} \rightarrow \vec{m})$  and permittivity is replaced by the inverse of permeability ( $\varepsilon_0 \rightarrow \frac{1}{\mu_0}$ ).



Fig. 11-6. (a) E-field lines far away from an electric dipole. (b) M-field lines far away from a magnetic dipole. (c) Close-up view of (a). (d) Close-up view of (b) (after Inans).