

# Waveguide Coupler I

Class: Integrated Photonic Devices

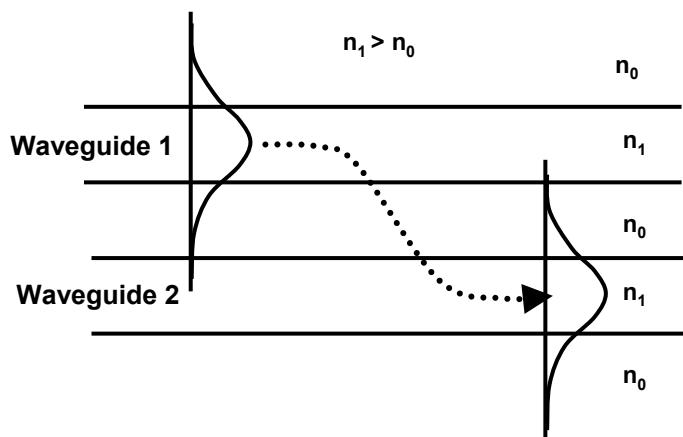
Time: Fri. 8:00am ~ 11:00am.

Classroom: 資電206

Lecturer: Prof. 李明昌(Ming-Chang Lee)

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## Waveguide Coupler

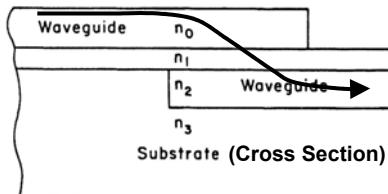


- How to switch the power from one waveguide to other waveguides

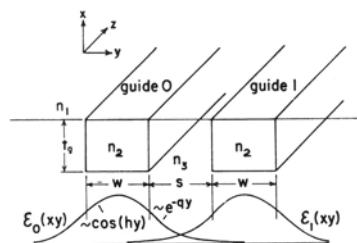
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## Two Types of Directional Couplers

### I. Planar Waveguide Coupler (Out-of-Plane)

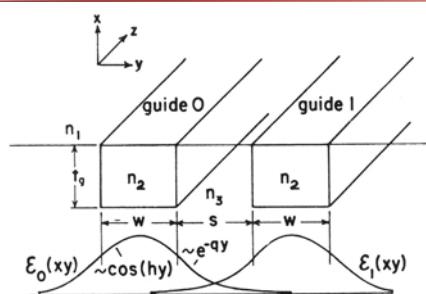


### II. Dual-Channel Waveguide Coupler (In-Plane)



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## Coupled Mode Theory for Directional Coupler



monochromatic waveguide modes

$$\vec{E}(x, y, z, t) = \hat{A}\hat{L}(z)\vec{\psi}(x, y)\exp(-j\omega t)$$

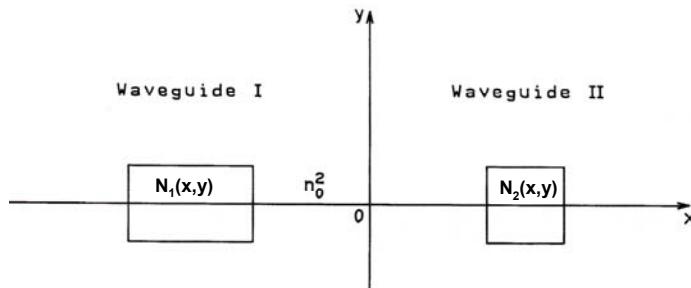
Axial (Longitudinal) Part      Transverse Part      Time harmonic

$\hat{L}(z)$  is a complex amplitude including phase term  $\exp(j\beta z)$

$\vec{\psi}(x, y)$  represents the field distribution of a single waveguide

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## Coupled Mode Theory for Directional Coupler



We define the eigen modes in each optical waveguide satisfying Maxwell's equations

$$\begin{cases} \nabla \times \tilde{\mathbf{E}}_p = j\omega\mu_0 \tilde{\mathbf{H}}_p \\ \nabla \times \tilde{\mathbf{H}}_p = -j\omega\epsilon_0 N_p^2 \tilde{\mathbf{E}}_p \end{cases} \quad (p=1,2) \quad N_p(x,y): \text{refractive index}$$

The electromagnetic fields of the coupled waveguide is summation of two eigen modes

$$\begin{cases} \tilde{\mathbf{E}} = A_1(z)\tilde{\mathbf{E}}_1 + A_2(z)\tilde{\mathbf{E}}_2 \\ \tilde{\mathbf{H}} = A_1(z)\tilde{\mathbf{H}}_1 + A_2(z)\tilde{\mathbf{H}}_2 \end{cases} \quad A_1 \text{ and } A_2 \text{ is the amplitude of optical fields}$$

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## Coupled Mode Theory for Directional Coupler

The summed fields should also satisfy Maxwell's equation

$$\begin{cases} \nabla \times \tilde{\mathbf{E}} = j\omega\mu_0 \tilde{\mathbf{H}} \\ \nabla \times \tilde{\mathbf{H}} = -j\omega\epsilon_0 N^2 \tilde{\mathbf{E}} \end{cases} \quad (1) \quad N(x,y) \text{ denote the entire refractive index of coupled waveguide}$$

The vector formula

$$\nabla \times (A\mathbf{E}) = A\nabla \times \mathbf{E} + \nabla A \times \mathbf{E} = A\nabla \times \mathbf{E} + \frac{dA}{dz} \mathbf{u}_z \times \mathbf{E} \quad (2)$$

(the amplitude only varies at z-direction) Perturbation!

Combine (1) and (2)

$$\left\{ \begin{array}{l} (\mathbf{u}_z \times \tilde{\mathbf{E}}_1) \frac{dA_1}{dz} + (\mathbf{u}_z \times \tilde{\mathbf{E}}_2) \frac{dA_2}{dz} = 0 \end{array} \right. \quad (3)$$

$$\left\{ \begin{array}{l} (\mathbf{u}_z \times \tilde{\mathbf{H}}_1) \frac{dA_1}{dz} + j\omega\epsilon_0(N^2 - N_1^2)A_1 \tilde{\mathbf{E}}_1 + (\mathbf{u}_z \times \tilde{\mathbf{H}}_2) \frac{dA_2}{dz} + j\omega\epsilon_0(N^2 - N_2^2)A_2 \tilde{\mathbf{E}}_2 = 0 \end{array} \right. \quad (4)$$

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## Coupled Mode Theory for Directional Coupler

$$\left\{ \begin{array}{l} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \left[ \tilde{\mathbf{E}}_1^* \cdot (4) - \tilde{\mathbf{H}}_1^* \cdot (3) \right] dx dy = 0 \\ \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \left[ \tilde{\mathbf{E}}_2^* \cdot (4) - \tilde{\mathbf{H}}_2^* \cdot (3) \right] dx dy = 0 \end{array} \right. \quad (5)$$

$$\left\{ \begin{array}{l} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \left[ \tilde{\mathbf{E}}_1^* \cdot (4) - \tilde{\mathbf{H}}_1^* \cdot (3) \right] dx dy = 0 \\ \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \left[ \tilde{\mathbf{E}}_2^* \cdot (4) - \tilde{\mathbf{H}}_2^* \cdot (3) \right] dx dy = 0 \end{array} \right. \quad (6)$$

From Eq. (5)

$$\begin{aligned} \frac{dA_1}{dz} + \frac{dA_2}{dz} & \cdot \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{u}_z \cdot (\tilde{\mathbf{E}}_1^* \times \tilde{\mathbf{H}}_2 + \tilde{\mathbf{E}}_2 \times \tilde{\mathbf{H}}_1^*) dx dy \\ & + jA_1 \frac{\omega \epsilon_0 \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} (N^2 - N_1^2) \tilde{\mathbf{E}}_1^* \cdot \tilde{\mathbf{E}}_1 dx dy}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{u}_z \cdot (\tilde{\mathbf{E}}_1^* \times \tilde{\mathbf{H}}_1 + \tilde{\mathbf{E}}_1 \times \tilde{\mathbf{H}}_1^*) dx dy} \\ & + jA_2 \frac{\omega \epsilon_0 \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} (N^2 - N_2^2) \tilde{\mathbf{E}}_2^* \cdot \tilde{\mathbf{E}}_2 dx dy}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{u}_z \cdot (\tilde{\mathbf{E}}_1^* \times \tilde{\mathbf{H}}_1 + \tilde{\mathbf{E}}_1 \times \tilde{\mathbf{H}}_1^*) dx dy} = 0 \end{aligned} \quad (7)$$

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## Coupled Mode Theory for Directional Coupler

From Eq. (6)

$$\begin{aligned} \frac{dA_2}{dz} + \frac{dA_1}{dz} & \cdot \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{u}_z \cdot (\tilde{\mathbf{E}}_2^* \times \tilde{\mathbf{H}}_1 + \tilde{\mathbf{E}}_1 \times \tilde{\mathbf{H}}_2^*) dx dy \\ & + jA_2 \frac{\omega \epsilon_0 \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} (N^2 - N_2^2) \tilde{\mathbf{E}}_2^* \cdot \tilde{\mathbf{E}}_2 dx dy}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{u}_z \cdot (\tilde{\mathbf{E}}_2^* \times \tilde{\mathbf{H}}_2 + \tilde{\mathbf{E}}_2 \times \tilde{\mathbf{H}}_2^*) dx dy} \\ & + jA_1 \frac{\omega \epsilon_0 \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} (N^2 - N_1^2) \tilde{\mathbf{E}}_1^* \cdot \tilde{\mathbf{E}}_1 dx dy}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{u}_z \cdot (\tilde{\mathbf{E}}_2^* \times \tilde{\mathbf{H}}_2 + \tilde{\mathbf{E}}_2 \times \tilde{\mathbf{H}}_2^*) dx dy} = 0 \end{aligned} \quad (8)$$

Here we separate the transverse and axial dependencies of electromagnetic fields

$$\left\{ \begin{array}{l} \tilde{\mathbf{E}}_p = \mathbf{E}_p \exp(j\beta_p z) \\ \tilde{\mathbf{H}}_p = \mathbf{H}_p \exp(j\beta_p z) \end{array} \right. \quad (p = 1, 2)$$

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## Coupled Mode Theory for Directional Coupler

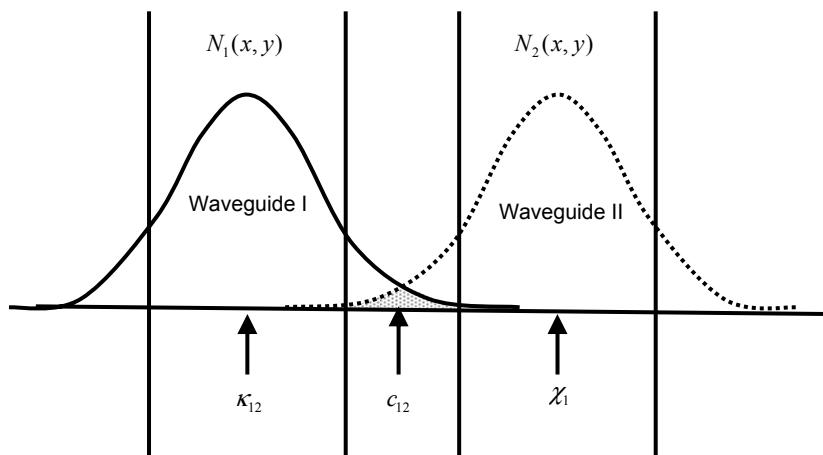
$$\left\{ \begin{array}{l} \frac{dA_1}{dz} + c_{12} \frac{dA_2}{dz} \exp[j(\beta_2 - \beta_1)z] + j\chi_1 A_1 + j\kappa_{12} A_2 \exp[j(\beta_2 - \beta_1)z] = 0 \quad (9) \text{ (from (7))} \\ \frac{dA_2}{dz} + c_{21} \frac{dA_1}{dz} \exp[-j(\beta_2 - \beta_1)z] + j\chi_2 A_2 + j\kappa_{21} A_1 \exp[-j(\beta_2 - \beta_1)z] = 0 \quad (10) \text{ (from (8))} \end{array} \right.$$

where

$$\left\{ \begin{array}{l} \kappa_{pq} = \frac{\omega \epsilon_0 \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} (N^2 - N_q^2) \mathbf{E}_p^* \cdot \mathbf{E}_q dxdy}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{u}_z \cdot (\mathbf{E}_p^* \times \mathbf{H}_p + \mathbf{E}_p \times \mathbf{H}_p^*) dxdy} \quad (\mathbf{q} \text{ perturb } \mathbf{p}) \\ c_{pq} = \frac{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{u}_z \cdot (\mathbf{E}_p^* \times \mathbf{H}_q + \mathbf{E}_q \times \mathbf{H}_p^*) dxdy}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{u}_z \cdot (\mathbf{E}_p^* \times \mathbf{H}_p + \mathbf{E}_p \times \mathbf{H}_p^*) dxdy} \quad (\mathbf{q} \text{ perturb } \mathbf{p}) \\ \chi_p = \frac{\omega \epsilon_0 \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} (N^2 - N_p^2) \mathbf{E}_p^* \cdot \mathbf{E}_p dxdy}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{u}_z \cdot (\mathbf{E}_p^* \times \mathbf{H}_p + \mathbf{E}_p \times \mathbf{H}_p^*) dxdy} \end{array} \right.$$

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## Coupled Mode Theory for Directional Coupler



- $\chi$  is much smaller than  $\kappa$

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## Coupled Mode Theory for Directional Coupler

(a). Consider  $\chi_p$

$$\chi_p = \chi_p^* \longrightarrow \chi_p \text{ is real number}$$

(b). Consider  $c_{pq}$

Recall

$$P_p = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{1}{2} \operatorname{Re}(\mathbf{E}_p \times \mathbf{H}_p^*) \cdot \mathbf{u}_z dx dy$$

$$\bar{E} = \frac{1}{2} (\bar{\mathbf{E}} \exp(-j\omega t) + \bar{\mathbf{E}}^* \exp(j\omega t))$$

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} (\mathbf{E}_p^* \times \mathbf{H}_p + \mathbf{E}_p \times \mathbf{H}_p^*) \cdot \mathbf{u}_z dx dy = 4P_p = 4$$

$$\bar{H} = \frac{1}{2} (\bar{\mathbf{H}} \exp(-j\omega t) + \bar{\mathbf{H}}^* \exp(j\omega t))$$

If  $\mathbf{E}_p, \mathbf{H}_p$  is the eigen mode

$$c_{pq} = \frac{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{u}_z \cdot (\mathbf{E}_p^* \times \mathbf{H}_q + \mathbf{E}_q \times \mathbf{H}_p^*) dx dy}{\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \mathbf{u}_z \cdot (\mathbf{E}_p^* \times \mathbf{H}_p + \mathbf{E}_p \times \mathbf{H}_p^*) dx dy} \longrightarrow c_{21} = c_{12}^*$$

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## Coupled Mode Theory for Directional Coupler

(c). Consider  $\kappa_{pq}$

Suppose there is no coupling loss, the total power should be constant

$$P = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{1}{2} \operatorname{Re}(\tilde{\mathbf{E}} \times \tilde{\mathbf{H}}^*) \cdot \mathbf{u}_z dx dy \quad \text{and} \quad \frac{dP}{dz} = 0$$



$$jA_1^* A_2 (\kappa_{21}^* - \kappa_{12} - 2\delta c_{12}) \exp(-j2\delta z) - jA_1 A_2^* (\kappa_{21} - \kappa_{12}^* - 2\delta c_{12}^*) \exp(j2\delta z) = 0$$

where  $\delta = \frac{(\beta_2 - \beta_1)}{2}$

for every z

$$\kappa_{21} = \kappa_{12}^* + 2\delta c_{12}^*$$

- The coupling coefficients are complicate conjugated when
  - Two modes are in the same waveguide or  $\rightarrow \delta = \frac{\beta_2 - \beta_1}{2} = 0$
  - Two waveguides are phase matching

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## Coupled Mode Theory for Directional Coupler

General expression of coupled mode theory

$$\begin{cases} \frac{dA_1}{dz} = j\kappa_a A_2 \exp(j2\delta z) + j\gamma_a A_1 & [(9)-(10) \times c_{12} \exp(j2\delta z) = 0] \\ \frac{dA_2}{dz} = j\kappa_b A_1 \exp(-j2\delta z) + j\gamma_b A_2 & [(10)-(9) \times c_{21} \exp(-j2\delta z) = 0] \end{cases}$$

where  $\begin{cases} \kappa_a = \frac{\kappa_{12} - c_{12}\chi_2}{1 - |c_{12}|^2} \\ \kappa_b = \frac{\kappa_{21} - c_{12}^*\chi_1}{1 - |c_{12}|^2} \end{cases}$  and  $\begin{cases} \gamma_a = \frac{\kappa_{21}c_{12} - \chi_1}{1 - |c_{12}|^2} \\ \gamma_b = \frac{\kappa_{12}c_{12}^* - \chi_2}{1 - |c_{12}|^2} \end{cases}$

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## Coupled Mode Theory for Directional Coupler

In most cases, we suppose two waveguides are sufficient separated

$$\chi_{p,q} \sim 0 \quad \text{and} \quad C_{pq} \ll 1$$

Then

$$\kappa_{12} = \kappa_{21} \quad \text{and} \quad \gamma_a = \gamma_b = 0$$

The general coupled mode theory is simplified by

$$\begin{cases} \frac{dA_1}{dz} = j\kappa_{12} A_2 \exp[j(\beta_2 - \beta_1)z] \\ \frac{dA_2}{dz} = j\kappa_{21} A_1 \exp[-j(\beta_2 - \beta_1)z] \end{cases}$$

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## Coupled Mode Theory for Directional Coupler

The coupling between mode is given by the coupled mode equations for the amplitudes of the two modes (guide 1 and guide 2)

$$\begin{cases} \frac{d\hat{A}_1(z)}{dz} = j\beta_1 \hat{A}_1(z) + j\kappa_{12} \hat{A}_2(z) \\ \frac{d\hat{A}_2(z)}{dz} = j\beta_2 \hat{A}_2(z) + j\kappa_{21} \hat{A}_1(z) \end{cases}$$
$$\hat{A}_1 = A_1 \exp(j\beta_1 z)$$
$$\hat{A}_2 = A_2 \exp(j\beta_2 z)$$

$\beta_1$  : the propagation constant of guide 1  
 $\beta_2$  : the propagation constant of guide 2

$\kappa_{12}$  : the coupling coefficient from 2 to 1  
 $\kappa_{21}$  : the coupling coefficient from 1 to 2

In general,  $\kappa_{12}$  and  $\kappa_{21}$  are not equal. We suppose the coupling coefficients are approximated and real

$$\kappa_{21} = \kappa_{12} = \kappa$$

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## Solutions of Directional Coupler

$$\begin{cases} \hat{A}_1(z) = \left\{ \left[ \cos(gz) + j \frac{\delta}{g} \sin(gz) \right] \hat{A}_1(0) - j \frac{\kappa}{g} \sin(gz) \hat{A}_2(0) \right\} \exp(j(\beta_1 + \delta)z) \\ \hat{A}_2(z) = \left\{ -j \frac{\kappa}{g} \sin(gz) \hat{A}_1(0) + \left[ \cos(gz) + j \frac{\delta}{g} \sin(gz) \right] \hat{A}_2(0) \right\} \exp(j(\beta_2 - \delta)z) \end{cases}$$

Where  $g^2 \equiv \kappa^2 + \delta^2$  and  $\delta \equiv \frac{\beta_2 - \beta_1}{2}$

If the initial condition  $A_1(0) = 1$  and  $A_2(0) = 0$ , the solution is

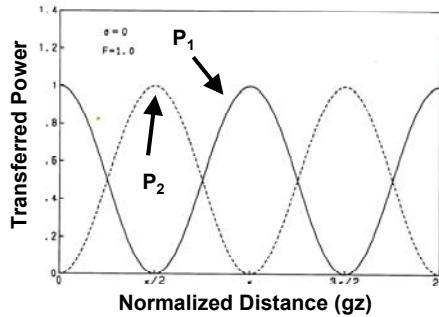
$$\begin{cases} \hat{A}_1(z) = \left[ \cos(gz) - j \frac{\delta}{g} \sin(gz) \right] \exp(j(\beta_1 + \delta)z) \\ \hat{A}_2(z) = j \frac{\kappa}{g} \sin(gz) \exp(j(\beta_2 - \delta)z) \end{cases}$$

- The propagation constant of each eigen mode becomes the average of two individual propagation constants in the coupling region

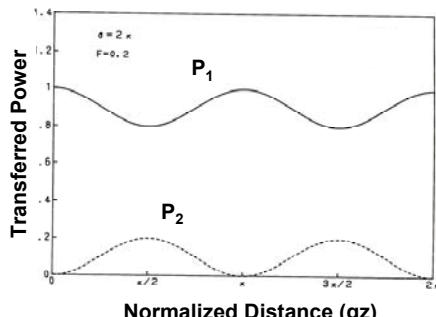
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## Transferred Power

### Phase Matching



### Phase Mismatching



$$\left\{ \begin{array}{l} \delta = 0 \\ P_1(z) = A_1(z) \cdot A_1(z)^* = \cos^2(gz) + \delta^2 \frac{\sin^2(gz)}{g^2} \\ P_2(z) = A_2(z) \cdot A_2(z)^* = \frac{\kappa^2}{g^2} \sin^2(gz) \end{array} \right.$$

Where  $g^2 \equiv \kappa^2 + \delta^2$  and  $\delta \equiv \frac{\beta_2 - \beta_1}{2}$

- With a phase difference  $\delta$ , the power transfer is incomplete

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## Directional Coupler with Phase Matching

Suppose the two waveguides are identical

$$\beta_1 = \beta_2 = \beta$$

and

$$\kappa_{21} = \kappa_{12} = \kappa$$

Real

The coupled mode equation becomes

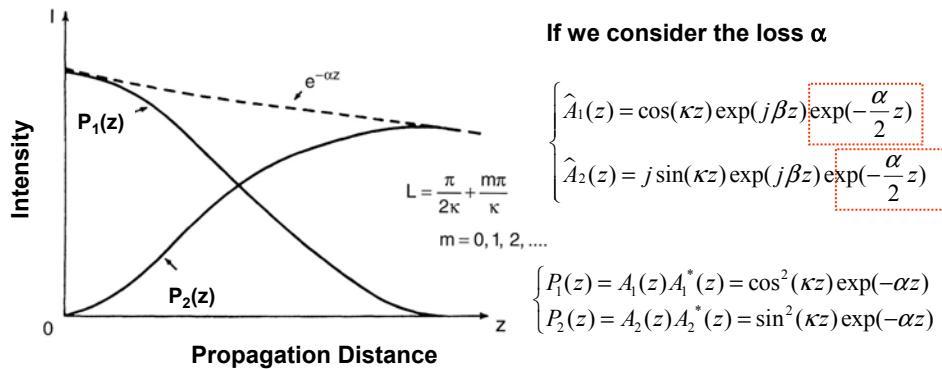
$$\left\{ \begin{array}{l} \frac{d\hat{A}_1(z)}{dz} = j\beta\hat{A}_1(z) + j\kappa\hat{A}_2(z) \\ \frac{d\hat{A}_2(z)}{dz} = j\beta\hat{A}_2(z) + j\kappa\hat{A}_1(z) \end{array} \right.$$

If the initial condition  $A_1(0) = 1$  and  $A_2(0) = 0$ , the solution is

$$\left\{ \begin{array}{l} \hat{A}_1(z) = \cos(\kappa z) \exp(j\beta z) \\ \hat{A}_2(z) = j \sin(\kappa z) \exp(j\beta z) \end{array} \right.$$

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# Directional Coupler with Phase Matching and Loss



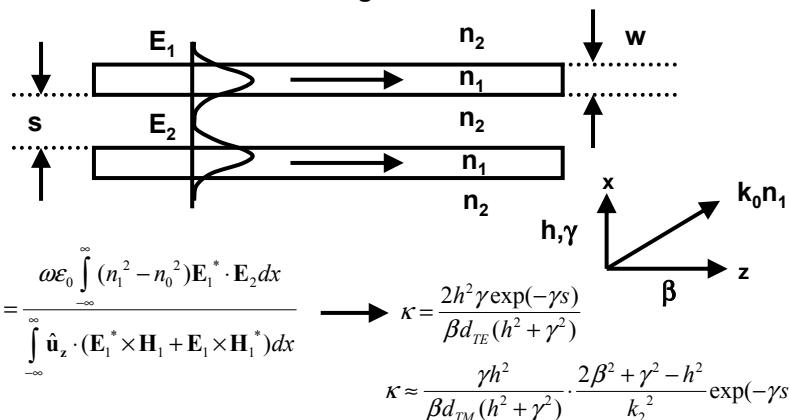
The optical power is completely transferred as propagation length (L)

$$L = \frac{(2m+1)\pi}{2\kappa}, m = 0, 1, 2, \dots$$

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## What is the coupling coefficient?

Suppose two identical slab waveguides

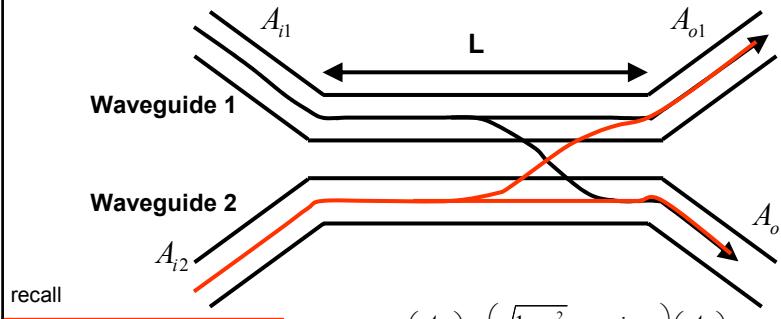


- The coupling coefficient is an exponential function of gap s.

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## Transfer Matrix Expression

Suppose a lossless coupler



$$\begin{pmatrix} A_{o1} \\ A_{o2} \end{pmatrix} = \begin{pmatrix} \sqrt{1-c^2} & jc \\ jc & \sqrt{1-c^2} \end{pmatrix} \begin{pmatrix} A_{i1} \\ A_{i2} \end{pmatrix}$$

$A_1(0)=1, A_2(0)=0$

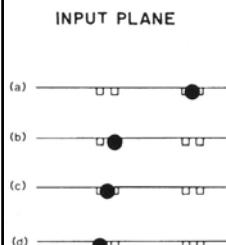
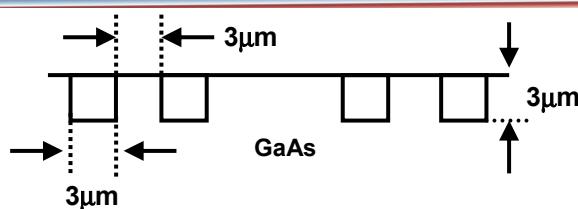
where  $c = \sin^2(\kappa L)$

$c^2$  : power coupling ratio

Varying L affects the power coupling ratio

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## Experimental Measurement



$L = 2.1 \text{ mm (100\% coupler)}$

$L = 1 \text{ mm (3dB coupler)}$

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## Summary of Waveguide Coupling

When you design a waveguide coupler, you have to

- Consider the coupling coefficient ( $\kappa$ )
- Consider the phase matching ( $\Delta\beta$ )
- Consider the coupling length (L)

$$\begin{cases} P_1(z) = \cos^2(gz) \exp(-\alpha z) + \delta^2 \frac{\sin^2(gz)}{g^2} \exp(-\alpha z) \\ P_2(z) = \frac{\kappa^2}{g^2} \sin^2(gz) \exp(-\alpha z) \end{cases}$$

$$g^2 \equiv \kappa^2 + \delta^2$$

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## Supermodes

Actually, the power oscillating between two waveguides can be thought as the beating between two supermodes.

For example, suppose the two waveguides are identical,

$$\begin{cases} \hat{A}_1(z) = A_0 \cos(\kappa z) \exp(j\beta z) \\ \hat{A}_2(z) = A_0 j \sin(\kappa z) \exp(j\beta z) \end{cases} \quad \text{if} \quad \begin{cases} \hat{A}_1(0) = A_0 \\ \hat{A}_2(0) = 0 \end{cases}$$

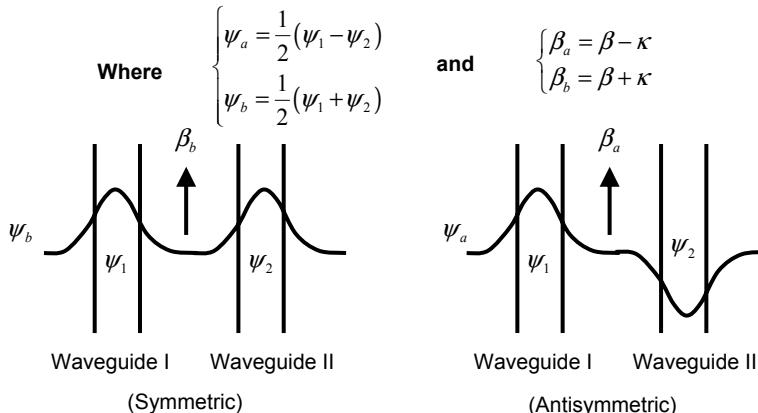
$$\begin{aligned} E(z) &= \hat{A}_1(z)\psi_1(x,y) + \hat{A}_2(z)\psi_2(x,y) \\ &= A_0 [\psi_1(x,y) \cos(\kappa z) \exp(j\beta z) + j\psi_2(x,y) \sin(\kappa z) \exp(j\beta z)] \\ &= A_0 \left\{ \frac{1}{2} \psi_1 [\exp(j\kappa z) + \exp(-j\kappa z)] \exp(j\beta z) + \frac{1}{2} \psi_2 [\exp(j\kappa z) - \exp(-j\kappa z)] \exp(j\beta z) \right\} \\ &= A_0 \underbrace{\left\{ \frac{1}{2} (\psi_1 - \psi_2) \exp[j(\beta - \kappa)z] + \frac{1}{2} (\psi_1 + \psi_2) \exp[j(\beta + \kappa)z] \right\}}_{E_a(z)} \underbrace{\left\{ \frac{1}{2} (\psi_1 + \psi_2) \exp[j(\beta + \kappa)z] - \frac{1}{2} (\psi_1 - \psi_2) \exp[j(\beta - \kappa)z] \right\}}_{E_b(z)} \end{aligned}$$

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## Supermodes

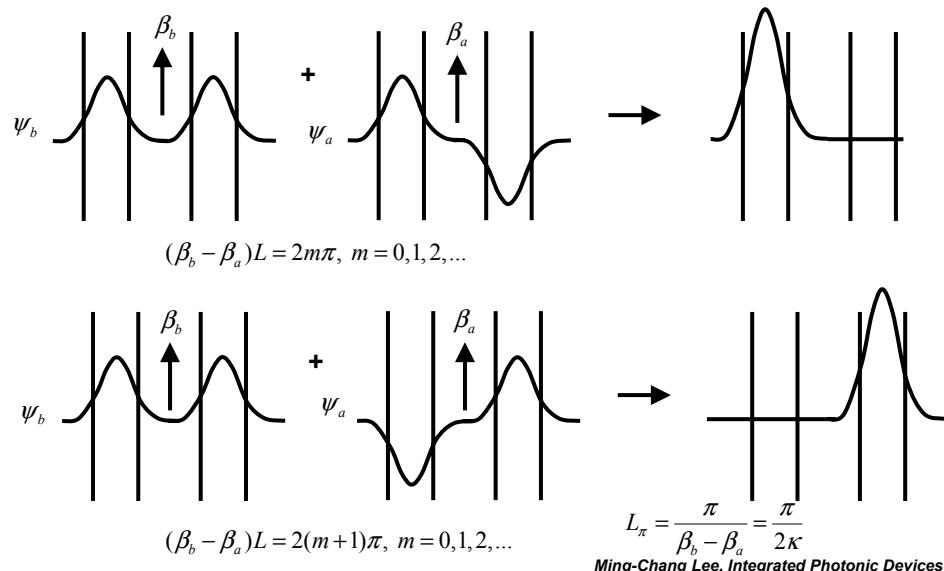
$$E(z) = A_0 \left\{ \frac{1}{2}(\psi_1 - \psi_2) \exp[j(\beta - \kappa)z] + \frac{1}{2}(\psi_1 + \psi_2) \exp[j(\beta + \kappa)z] \right\}$$

$$= A_0 \psi_a \exp(j\beta_a z) + A_0 \psi_b \exp(j\beta_b z) = A_0 E_a(z) + A_0 E_b(z)$$



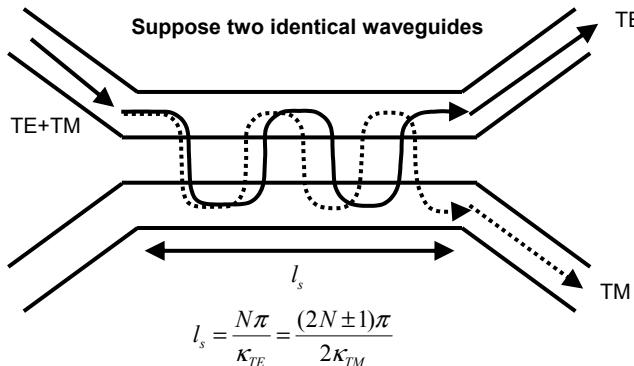
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## Supermodes



## Polarization Dependent

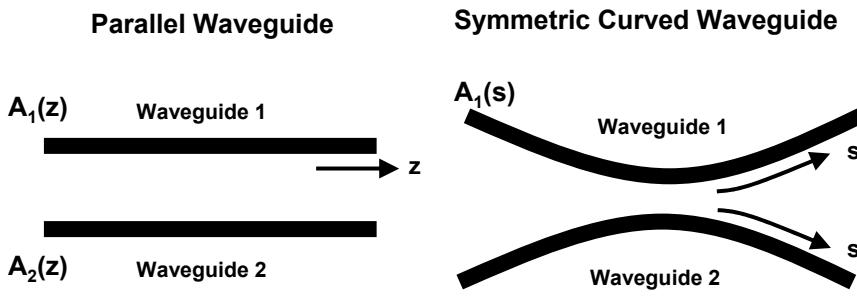
Because the coupling coefficients of TE modes and TM modes are different, we can design a polarization splitter.



where  $N$  :integer and  $\kappa_{TE}$   $\kappa_{TM}$  are coupling coefficient for TE and TM

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## Symmetric Curved Waveguide Coupling



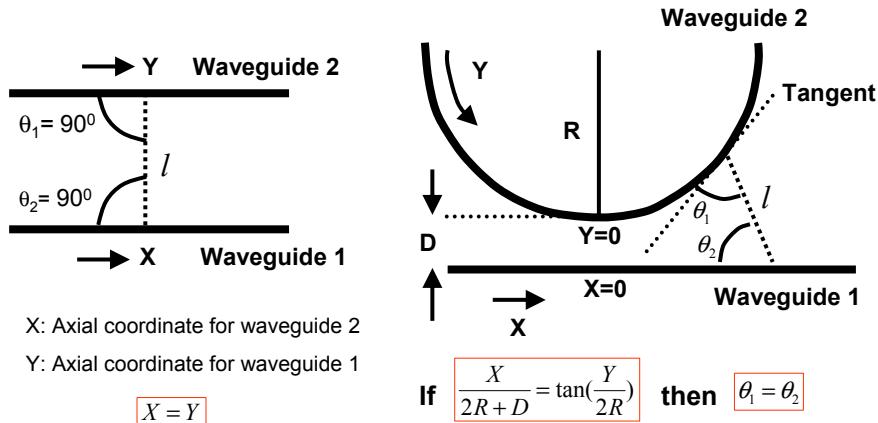
$$\begin{cases} d\hat{A}_1(z) = j\beta_1 \hat{A}_1(z)dz + j\kappa_{12} \hat{A}_2(z)dz \\ d\hat{A}_2(z) = j\beta_2 \hat{A}_2(z)dz + j\kappa_{21} \hat{A}_1(z)dz \end{cases}$$

$$\begin{cases} d\hat{A}_1(s) = j\beta_1 \hat{A}_1(s)ds + j\kappa_{12}(s) \hat{A}_2(s)ds \\ d\hat{A}_2(s) = j\beta_2 \hat{A}_2(s)ds + j\kappa_{21}(s) \hat{A}_1(s)ds \end{cases}$$

- Line coordinate vs. curve coordinate
- The amplitude increment can be modelled in point-to-point correspondence

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## Asymmetric Curved Waveguide Coupling



- If we can define a function to link X,Y curve coordinates such that  $\theta_1 = \theta_2$ , the asymmetric curved waveguide coupling can be treated as a symmetric curved waveguide coupling.

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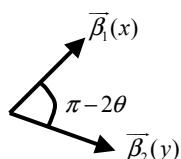
## Asymmetric Curved Waveguide Coupling

The asymmetric curved waveguide coupling can be expressed by coupled mode theory.

$$\begin{cases} d\hat{A}_1(x) = j\beta_1(x)\hat{A}_1(x)dx + j\tilde{\kappa}_2(y)\hat{A}_2(y)dy \\ d\hat{A}_2(y) = j\beta_2(y)\hat{A}_2(y)dy + j\tilde{\kappa}_1(x)\hat{A}_1(x)dx \end{cases}$$

where  $\frac{X}{2R+D} = \tan(\frac{Y}{2R})$  and

$$\begin{cases} \tilde{\kappa}_1 = \kappa_0 \cdot \cos(\pi - 2\theta) \cdot \left( \frac{dy}{dx} \right)^{1/2} \\ \tilde{\kappa}_2 = \kappa_0 \cdot \cos(\pi - 2\theta) \cdot \left( \frac{dx}{dy} \right)^{1/2} \end{cases}$$



Coupling coefficient due to gap

The angle of  $\overline{\beta}_1(x), \overline{\beta}_2(y)$

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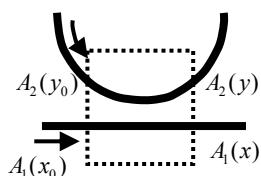
## Asymmetric Curved Waveguide Coupling

Consider the coupler is lossless; that is, the coupling power is conservative

$$\tilde{\kappa}_1 dx = \tilde{\kappa}_2 dy$$

The coupled mode theory becomes

$$\begin{cases} d\hat{A}_1(x) = j\beta_1(x)\hat{A}_1(x)dx + j\tilde{\kappa}_1(x)\hat{A}_2(y)dx \\ d\hat{A}_2(y) = j\beta_2(y)\hat{A}_2(y)dy + j\tilde{\kappa}_2(y)\hat{A}_1(x)dy \end{cases} \rightarrow \begin{cases} \frac{d\hat{A}_1(x)}{dx} = j\beta_1(x)\hat{A}_1(x) + j\tilde{\kappa}_1(x)\hat{A}_2(y) \\ \frac{d\hat{A}_2(y)}{dy} = j\beta_2(y)\hat{A}_2(y) + j\tilde{\kappa}_2(y)\hat{A}_1(x) \end{cases}$$



$$\begin{bmatrix} A_1(x) \\ A_2(y) \end{bmatrix} = \begin{bmatrix} C_{11}(x,y) & C_{12}(x,y) \\ C_{21}(x,y) & C_{22}(x,y) \end{bmatrix} \cdot \begin{bmatrix} A_1(x_0) \\ A_2(y_0) \end{bmatrix}$$

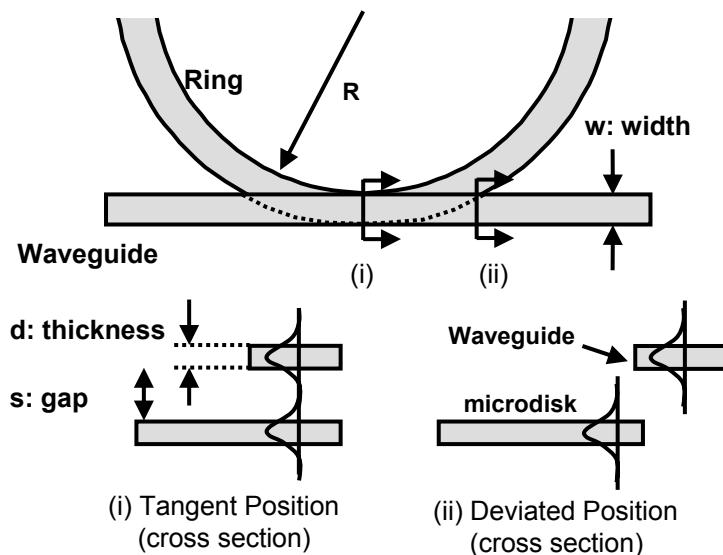
$$|C_{11}(x,y)|^2 + |C_{21}(x,y)|^2 = |C_{12}(x,y)|^2 + |C_{22}(x,y)|^2 = 1$$

$$C_{11}(x,y) \cdot C_{12}(x,y)^* + C_{21}(x,y) \cdot C_{22}(x,y)^* = 0$$

Due to power conservation

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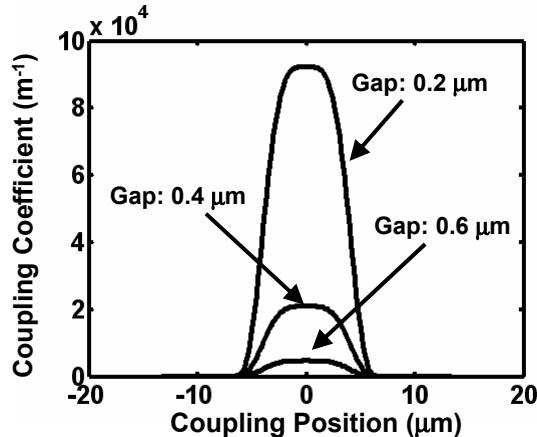
## Example of Asymmetric Curved Waveguide Coupling (Vertical Coupling)



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## Example of Asymmetric Curved Waveguide Coupling (Vertical Coupling)

For a silicon curved waveguide with 20- $\mu\text{m}$  radius of curvature and 0.8  $\mu\text{m}$  width, coupling coefficient ( $k_0$ ) is analyzed as follow:

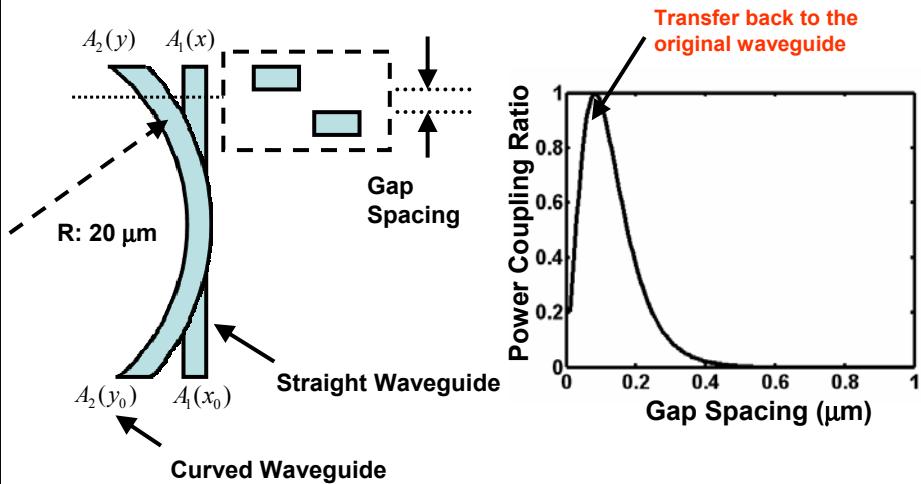


The effective coupling length is only from -5  $\mu\text{m}$  to 5  $\mu\text{m}$

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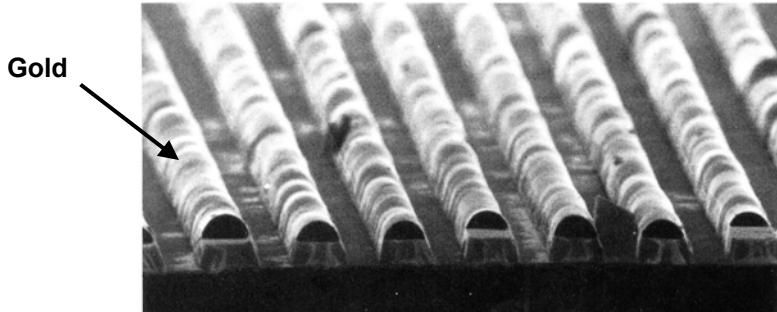
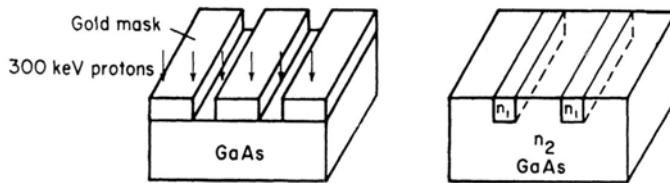
## Example of Asymmetric Curved Waveguide Coupling (Vertical Coupling)

Because the coupling coefficient is dependent on the gap spacing, the power coupling ratio is also a function of gap spacing.



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## Coupler Fabrication



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