

Distributed-Feedback Lasers

Class: Integrated Photonic Devices

Time: Fri. 8:00am ~ 11:00am.

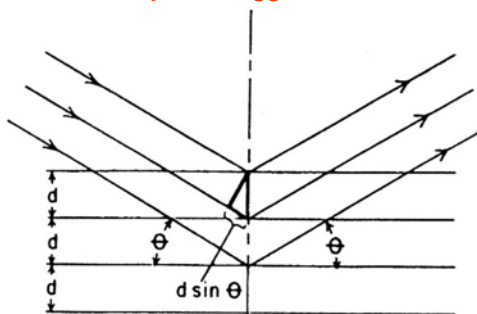
Classroom: 資電206

Lecturer: Prof. 李明昌(Ming-Chang Lee)

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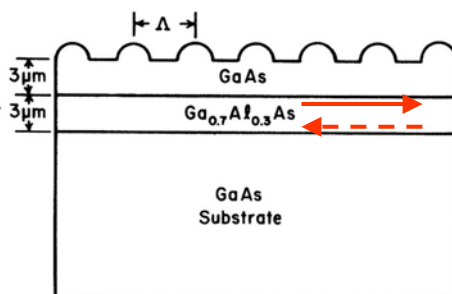
Wavelength Dependence of Bragg Reflections

Free-Space Bragg Reflection



$$2d \sin \theta = l\lambda \quad \text{and} \quad l = 1, 2, 3, \dots$$

Waveguide Bragg Reflection



Let $\theta = 90^\circ$

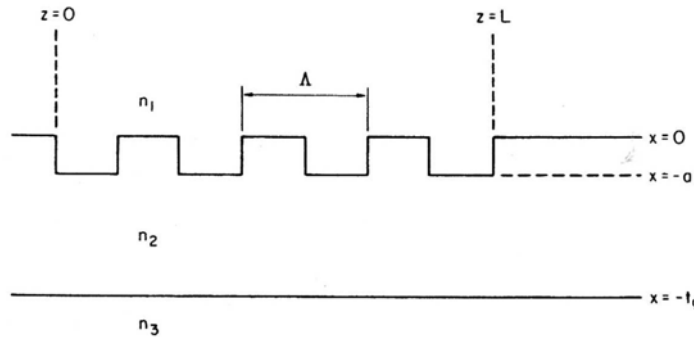
$$2\Lambda = l(\lambda_0 / n_e) \quad \text{and} \quad l = 1, 2, 3, \dots$$

Effective index

- Usually only one mode will lie within the gain bandwidth of the laser

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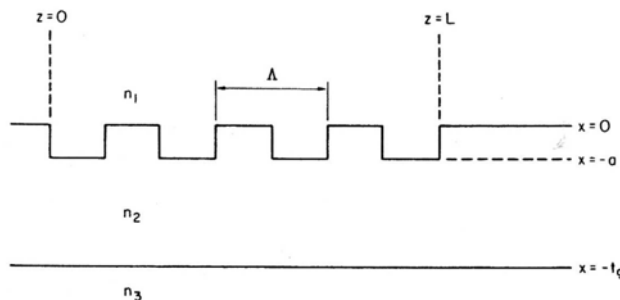
Coupling Efficiency of Wave Reflection



- The fraction of optical power that is reflected by a grating depends on
 - Thickness of the waveguiding layer
 - Depth of the grating teeth
 - Length of the grating region

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Coupling Efficiency of Wave Reflection



The coupling can be characterized by perturbation assumption

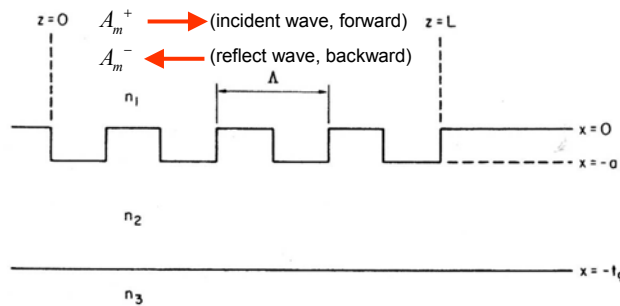
$$\kappa = \frac{2\pi^2}{3l\lambda_0} \frac{(n_2^2 - n_1^2)}{n_2} \left(\frac{a}{t_g} \right)^3 \left[1 + \frac{3(\lambda_0/a)}{2\pi(n_2^2 - n_1^2)^{1/2}} + \frac{3(\lambda_0/a)^2}{4\pi^2(n_2^2 - n_1^2)} \right]$$

where

$$l \approx \frac{\beta_m \Lambda}{\pi} \quad \beta_m \text{ is the propagation constant of the particular mode } m$$

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Coupling Efficiency of Wave Reflection



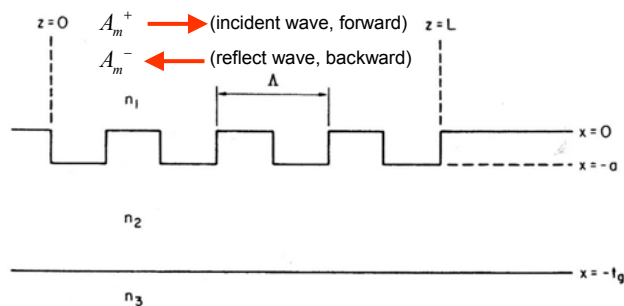
For the first order ($l=1$) case, the reflection is essentially limited to coupling between the forward and backward traveling wave

$$A_m^+(z) = A_m^+(0) \frac{\cosh[\kappa(z-L)]}{\cosh(\kappa L)} \quad \text{and} \quad A_m^-(z) = A_m^+(0) \frac{\kappa \sinh[\kappa(z-L)]}{|\kappa| \cosh(\kappa L)}$$

L : the length of grating

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Coupling Efficiency of Wave Reflection



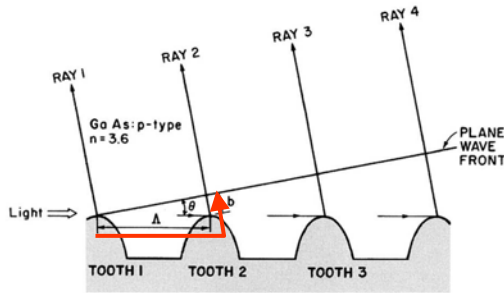
The reflectance and transmittance are

$$R_{eff} = \left| \frac{A_m^-(0)}{A_m^+(0)} \right|^2 \quad \text{and} \quad T_{eff} = \left| \frac{A_m^+(L)}{A_m^+(0)} \right|^2$$

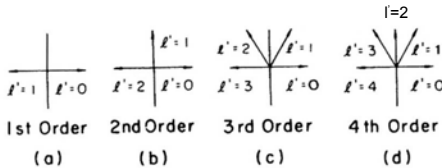
- The incident power decreases exponentially with z , as power is reflected into the backward travelling wave

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Ray Scattering of Higher-Order Bragg Gratings



Ga_{0.4}Al_{0.6}As: p-type
n=3.2



For higher-order gratings with periodicity Λ

$$\Lambda = \frac{l\lambda_0}{2n_e} \quad l > 0$$

The extra path length must be integral multiples of the wavelength to have constructive scattering ray

$$b + \Lambda = \frac{l'\lambda_0}{n_e} \quad l' = 0, 1, 2, 3, \dots, l$$

and

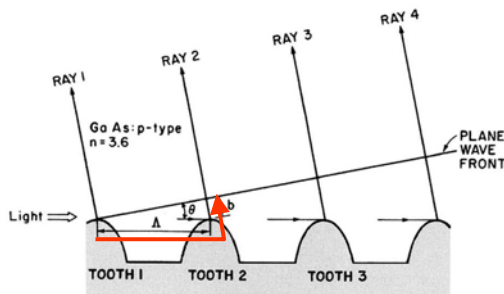
$$b = \Lambda \sin \theta$$

Thus,

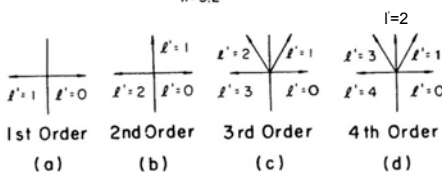
$$\sin \theta = \frac{l'\lambda_0}{n_e \Lambda} - 1 \quad l' = 0, 1, 2, 3, \dots, l$$

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Ray Scattering of Higher-Order Bragg Gratings



Ga_{0.4}Al_{0.6}As: p-type
n=3.2



For example of a second-order Bragg grating

$$\Lambda = \frac{\lambda_0}{n_e}$$

Then

$$\sin \theta = l' - 1 \quad l' = 0, 1, 2$$

Three diffraction modes

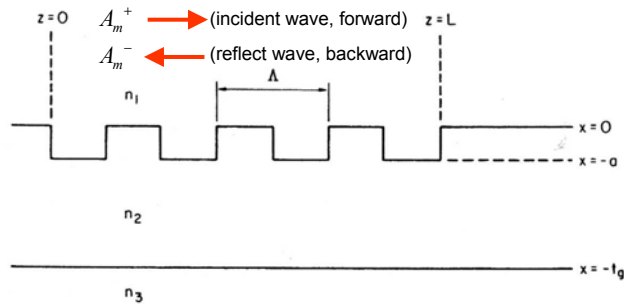
$$l' = 0 \quad \rightarrow$$

$$l' = 1 \quad \leftarrow$$

$$l' = 2 \quad \uparrow$$

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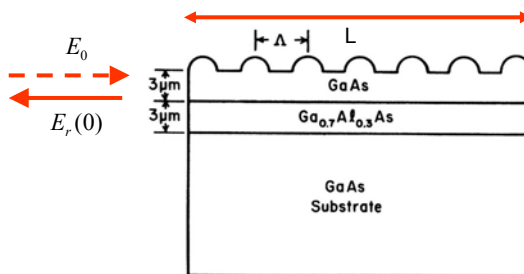
Coupling Efficiency of Wave Reflection



- Generally, the strong coupling in the transverse direction by second-order Bragg grating is undesirable
- A first-order grating is required to yield optimum performance
- However, fabrication of the first-order grating is challenging.

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Lasing with Distributed Feedback



In a gain medium (gain: g),

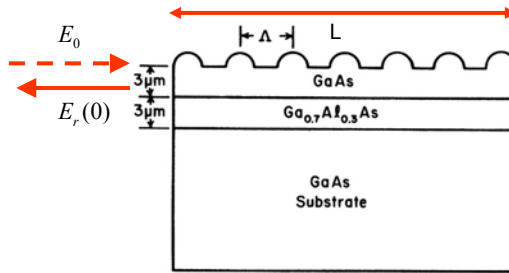
$$E_r(z) = E_0 \frac{\kappa \exp(j\beta_0 z) \sinh[S(L-z)]}{(g - j\Delta\beta) \sinh(SL) - S \cosh(SL)}$$

$$\text{where } S^2 \equiv |\kappa|^2 + (g - j\Delta\beta)^2$$

The parameter E_0 is the amplitude of a single mode incident on the grating (stimulus)

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Lasing with Distributed Feedback



The phase mismatching term,

$$\Delta\beta = \beta - \beta_0 \quad \text{Where } \beta_0 \text{ is the propagation constant at the Bragg wavelength}$$

The oscillation condition for the DFB laser corresponds to the case for

$$\frac{E_r(0)}{E_0} \rightarrow \infty$$

That is,

$$(g - j\Delta\beta) \sinh(SL) = S \cosh(SL)$$

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Lasing with Distributed Feedback

In general, numerical method should be used for exactly solving g and $\Delta\beta$ simultaneously. A special case of solution of lasing frequency

$$\omega_m = \omega_0 - \left(m + \frac{1}{2}\right) \frac{\pi c}{n_g L} \quad m = 0, \pm 1, \pm 2, \dots \quad \Delta\beta \equiv \beta - \beta_0 \approx \frac{(\omega - \omega_0) n_g}{c}$$

Supposing that $g \gg |\kappa|, \Delta\beta$ ω_0 : Bragg Frequency

It is interesting to note that no oscillation can occur at exactly the Bragg frequency ω_0 . The mode spacing

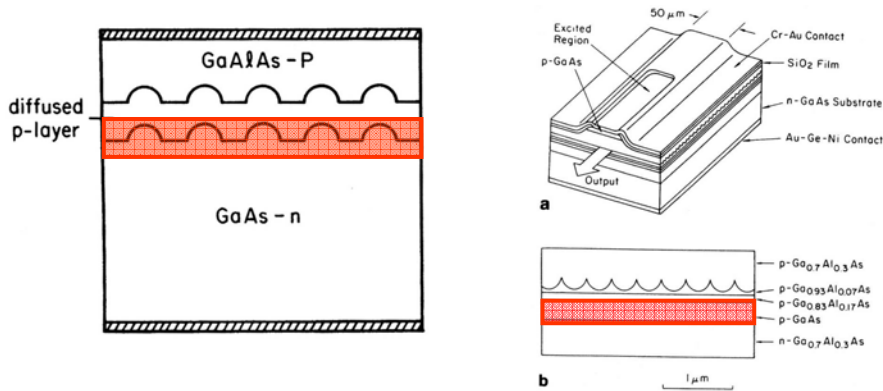
$$\Delta\omega_m \approx \frac{\pi c}{n_g L}$$

However, only the lasing modes close to the Bragg frequency have the smallest threshold gain. Therefore, in a normal operating condition, the spectral feature of DFB laser often consists of the two longitudinal modes

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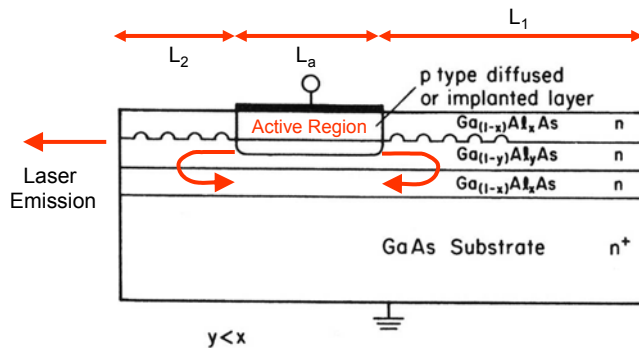
Separate Confinement Heterostructure Lasers

- Lattice damage is usually created during the grating fabrication.
→ It is better to separate the active layer out of the grating layer



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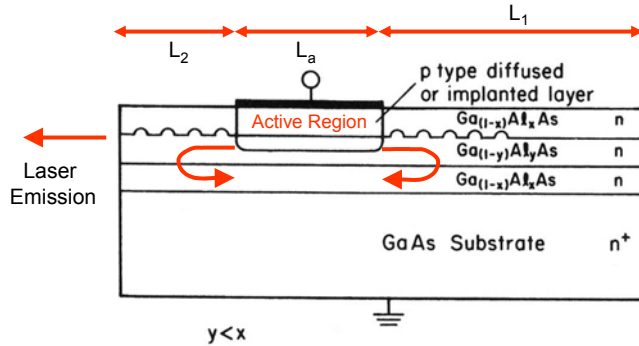
Distributed Bragg Reflection Lasers



- Two Bragg gratings are employed at both ends of the laser and outside of the electrically-pumped active region
- To achieve a single longitudinal mode, one distributed reflector must have narrow bandwidth, high reflectivity at the lasing wavelength

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Distributed Bragg Reflection Lasers



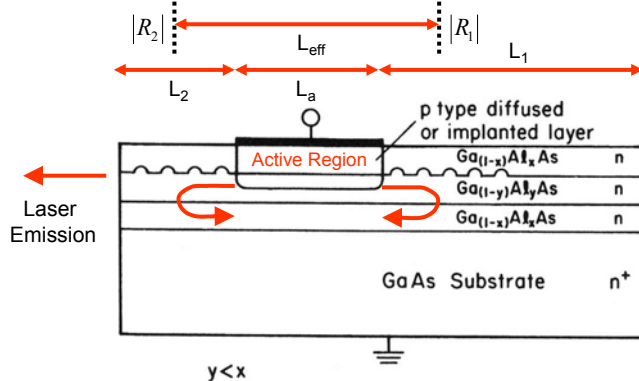
For the passive grating region,

The Transmittivity: $T = \frac{\gamma \exp[-j(\beta - \Delta\beta)L]}{(\alpha + j\Delta\beta) \sinh(\gamma L) + \gamma \cosh(\gamma L)}$ where $\gamma^2 \equiv \kappa^2 + (\alpha + j\Delta\beta)^2$

The Reflectivity: $R = \frac{-j\kappa \sinh(\gamma L)}{(\alpha + j\Delta\beta) \sinh(\gamma L) + \gamma \cosh(\gamma L)}$ (complex) Loss of grating

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Distributed Bragg Reflection Lasers

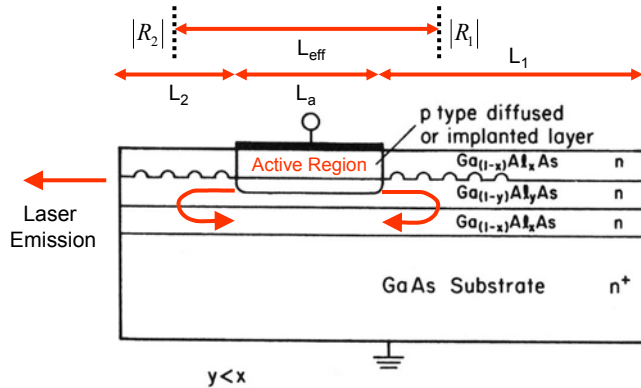


Since the reflectivity is complex number, we can consider an effective cavity length

$$L_{eff} = L_a \left(1 + \frac{L_2}{2L_a(\alpha L_1 + 1)} + \frac{1}{2L_a(\alpha + \sqrt{\kappa^2 + \alpha^2})} \right)$$

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Distributed Bragg Reflection Lasers

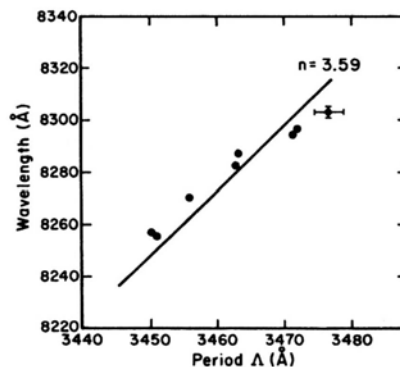


The longitudinal mode spacing between the m -th and $(m \pm 1)$ -th lasing mode is approximately

$$\Delta \equiv |\beta_m - \beta_{m \pm 1}| = \frac{\pi}{L_{eff}}$$

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Wavelength Selectability



- Compared with Fabry-Perot lasers, DFB or DBR laser is easy to achieve single-longitudinal-mode operation because the spacing between the m -th and the $(m \pm 1)$ -th mode is generally large and the reflectivity is mode-dependent

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