

A dark, high-contrast image of a circuit board with intricate patterns of lines and dots, serving as a background for the chapter title.

CHAPTER 4

Smart Imaging

Outline

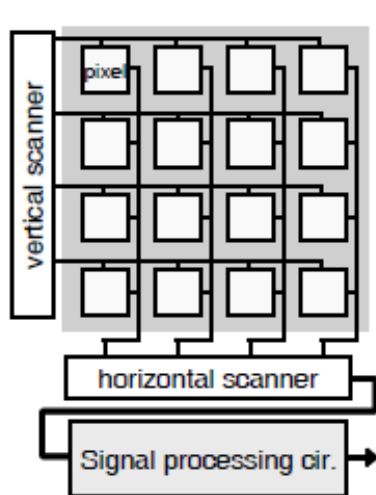
- 4.1 introduction
- 4.2 Low light imaging
- 4.3 High speed
- 4.4 Wide dynamic range
- 4.5 Demodulation
- 4.6 Three dimensional range finder
- 4.7 Target tracking
- 4.8 Dedicated arrangement of pixel and optics

Outline

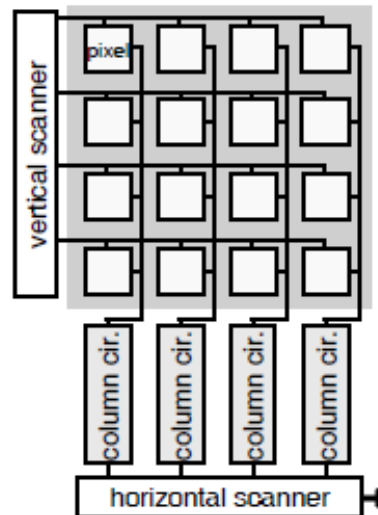
- 4.1 introduction
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Types of Implementation

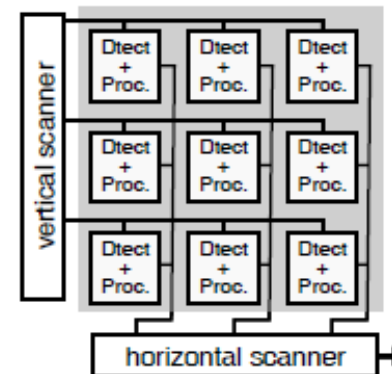
- Basic concept of smart CMOS image sensors
 - (a) chip-level processing
 - (b) column-level processing
 - (c) pixel-level processing



(a)



(b)



(c)

Other Features

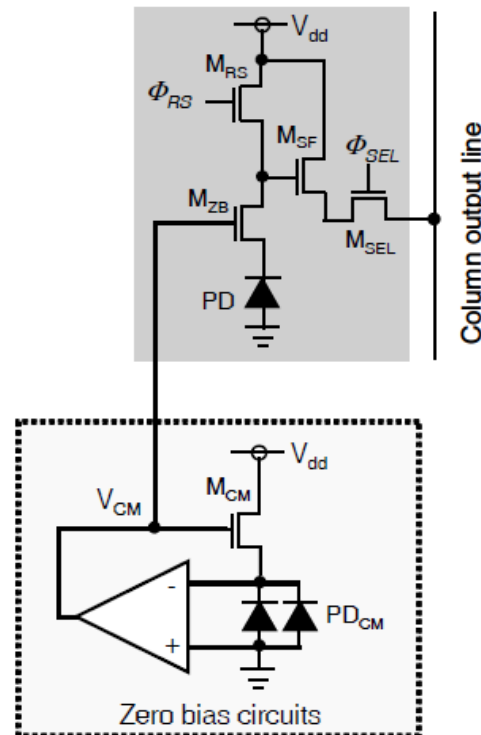
- Random access to an arbitrary pixel
- Non-destructive readout or multiple readout
(Note that the original 4T-APS cannot be applied for non-destructive readout)
- Integration of signal processing circuitry in each pixel and/or each column and/or a chip

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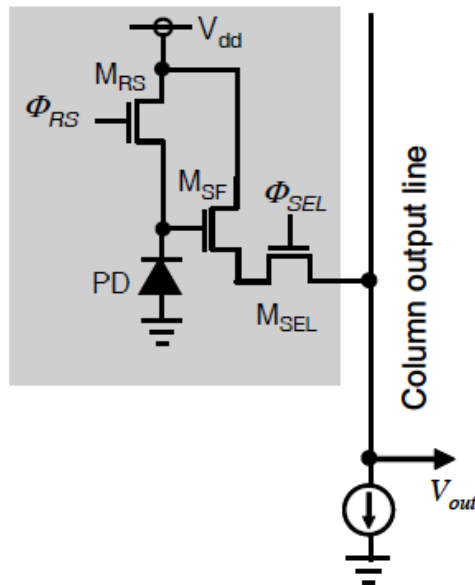
Reducing Dark Current

- Cooling
- Near zero bias circuits for reducing dark current in an APS

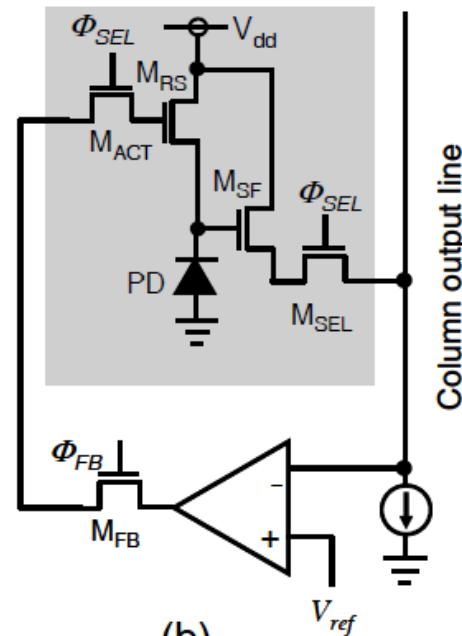


Active Reset

- Active reset circuits
 - (a) conventional 3T-APS
 - (b) 3T-APS with active reset

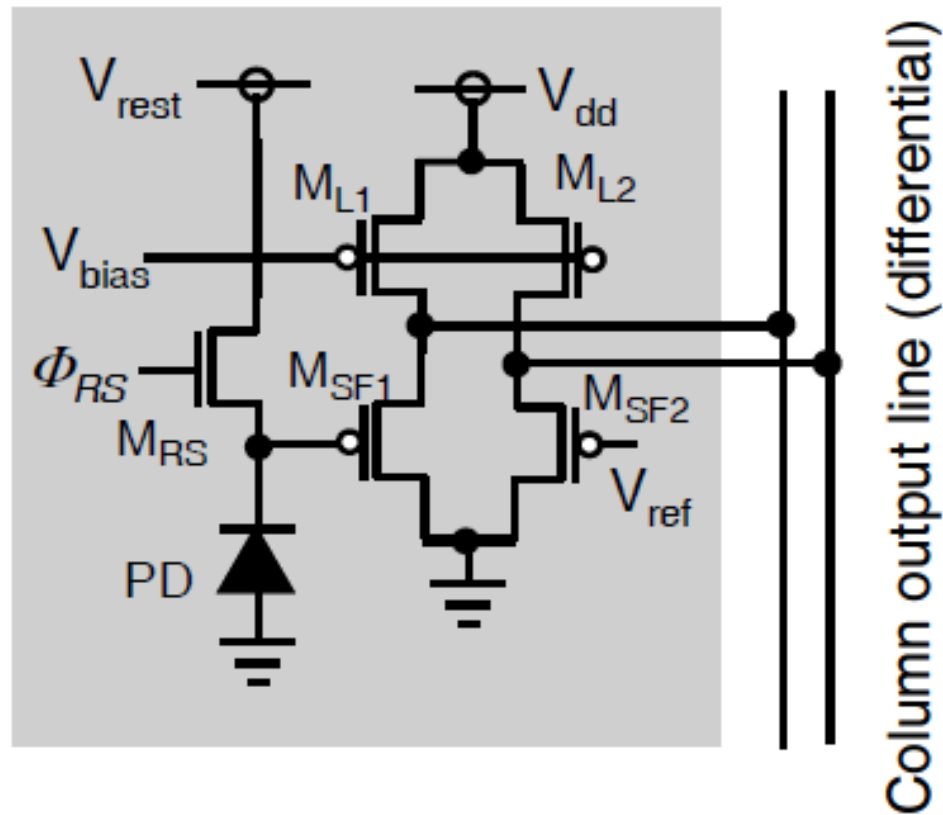


(a)



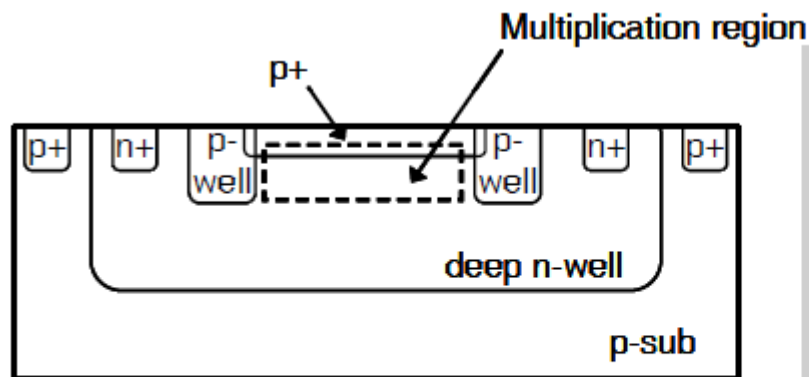
(b)

Differential APS

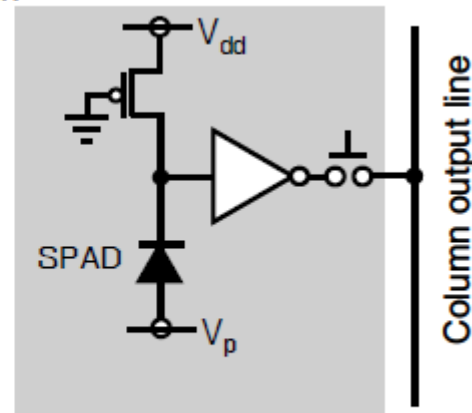


Geiger Mode APD

- SPAD: single photon avalanche diode.
 - Spike-like signal, not analog output
 - Produced pulse count proportional to light intensity



(a)



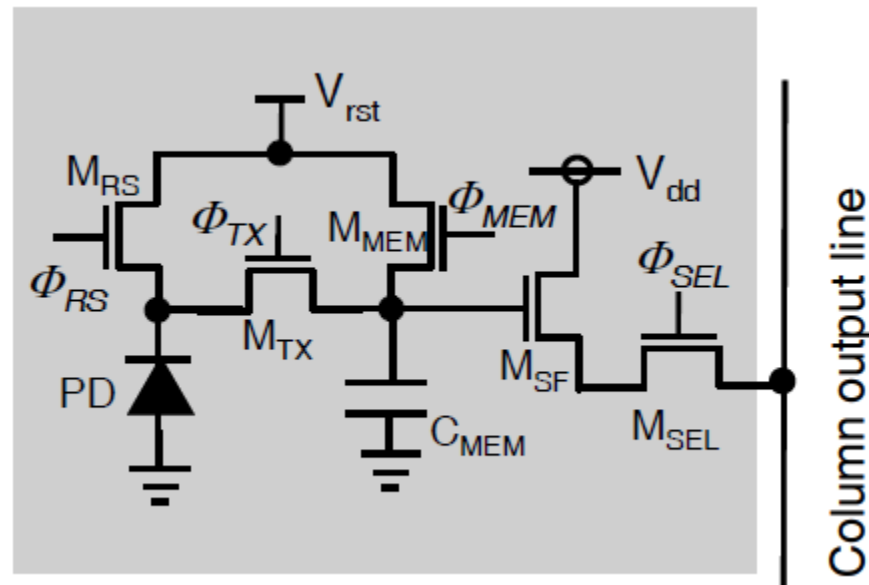
(b)

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Global Shutter

- Image lag is critical for frame rate $> 1000\text{fps}$
- 4T-APS is not suitable due to long transfer time
- Hard reset is necessary
- Global shutter



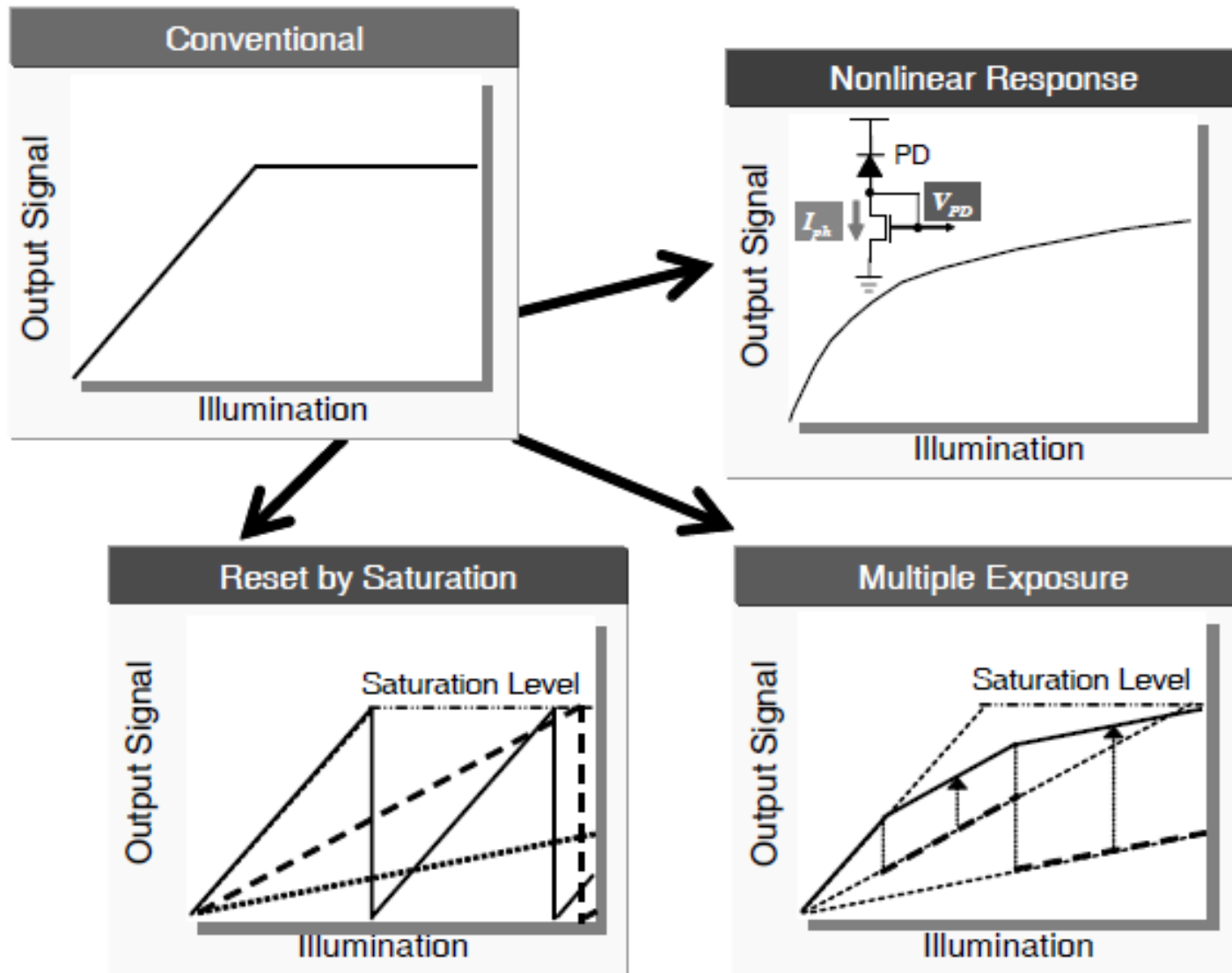
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Wide Dynamic Range

- Human eye : 200dB
 - 2 sensing cell : cone & rods
 - Nonlinear response
- Conventional CIS : 60-70dB
- Security/automobile requirement : >100dB
- WDR approaches
 - Nonlinear response
 - Multiple exposure
 - Saturation detection

Enhancing Dynamic Range



Synthesized WDR Image



Smart CMOS Sensors for WDR

Category	Implementation method	Refs.
Dual sensitivity	PG & PD in a pixel	[302, 306, 307]
Nonlinear response	Log sensor	[163–169]
	Log/linear response	[308–310]
	Well capacity adjustment	[298, 311–318]
	Control integration time/gain	[319, 320]
Multiple sampling	Dual sampling	[321–323]
	Multiple sampling with fixed short exposure time	[324, 325]
	Multiple sampling with varying short exposure time	[301]
	Multiple sampling with pixel-level ADC	[140, 184, 186]
Saturation detection	Locally integration time and gain	[326]
	Saturation count	[263, 326–332]
	Pulse width modulation	[179, 263, 333]
	Pulse frequency modulation	[141, 194, 196, 202, 334, 335]
Diffusive brightness	Resistive network	[304, 305]

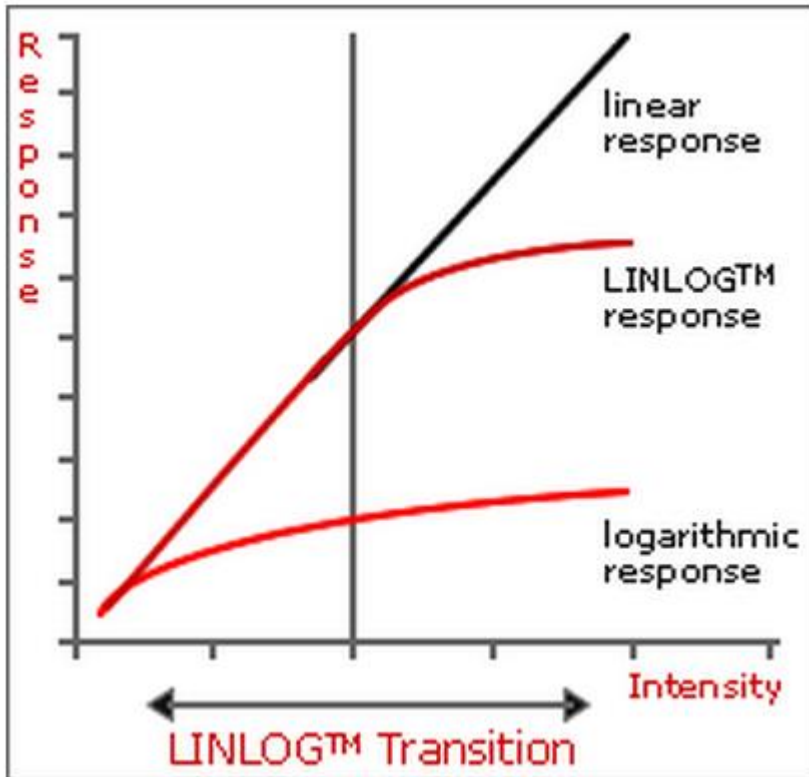
Dual Sensitivity

- Two PD : Higher & lower sensitivity
 - Mimic human eye
- In 4T-APS, FD can be used as lower sensitivity diode.
 - Synchronized high/low illuminated signal capture
 - No timing latency

Log Sensor

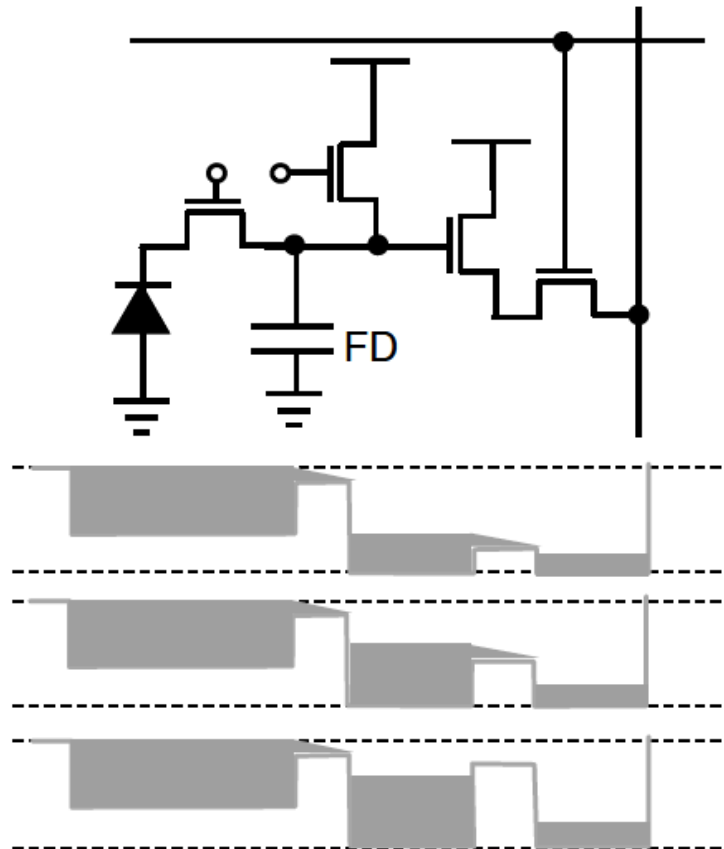
- Nonlinear response
- Small signal at low light
- Slow response
- Fixed pattern noise
- Linear-Log (LinLog) sensor
 - Linear response for low illumination
 - Log response for high illumination
 - Need calibration in the transition region

LinLog Sensor



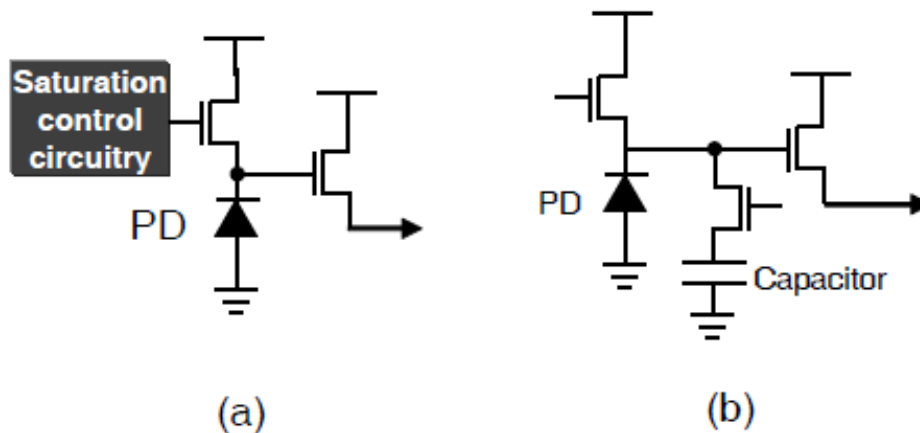
Well-Capacity Adjustment

- Overflow control for high illumination
- Stacked capacitor to increase well capacity (DR)



Reset Control & Extra Cap.

- Different approaches for WDR
 - (a) method to control the reset transistor
 - (b) method to use another accumulation capacitor



Dual Sampling

- Multiple readout scheme for wide dynamic range
 - Long exposure T_l for low-illuminated object
 - Short exposure T_s for high-illuminated object
 - Need synthesis to combine images
 - SNR drop issue

$$I_{\max} \cdot T_s = Q_{\max}, \quad I_{\min} \cdot T_l = Q_{\min}, \quad T_l = T_f - T_s$$

$$DR = 20 \log \frac{I_{\max}}{I_{\min}} = 20 \log \frac{Q_{\max} T_l}{Q_{\min} T_s} = DR_{org} + 20 \log \left(\frac{T_f}{T_s} - 1 \right)$$

Multiple Sampling

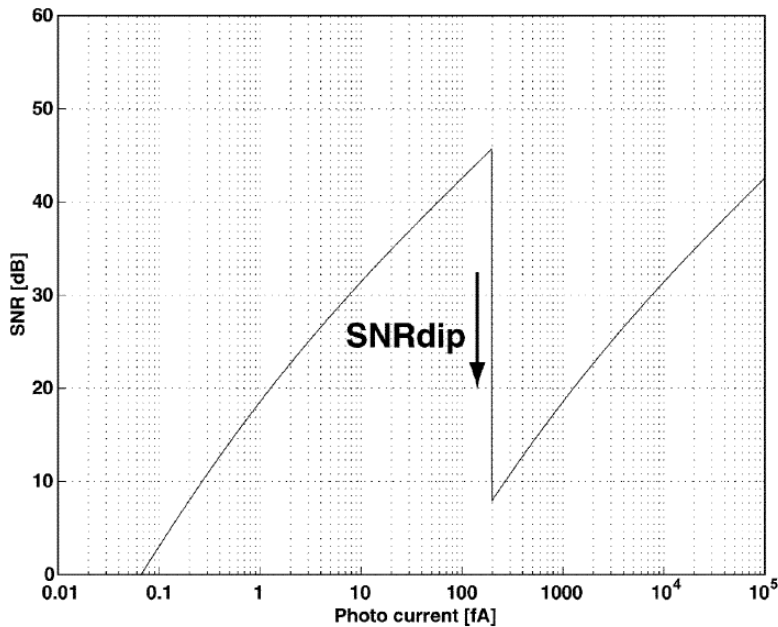
- Fixed short time exposure
 - T_l =integration time
 - T_f =frame time
 - T_s =short integration time
 - k =number of reading the short time integration
($k=1$ is Double sampling)
- SNR dip at boundary of exp.
- Dynamic range expansion

$$T_l = T_f - kT_s.$$

$$\Delta SNR = 10 \log k \frac{T_s}{T_l}.$$

$$\Delta DR = 20 \log \left(\frac{T_f}{T_s} - k \right)$$

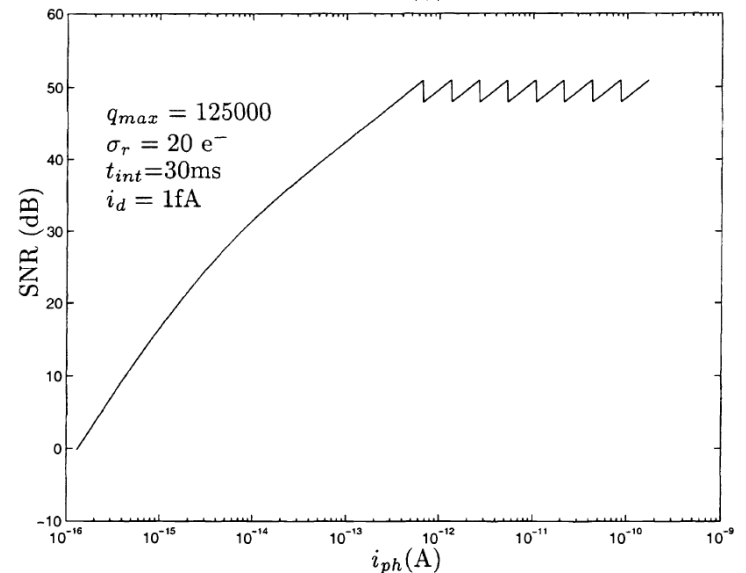
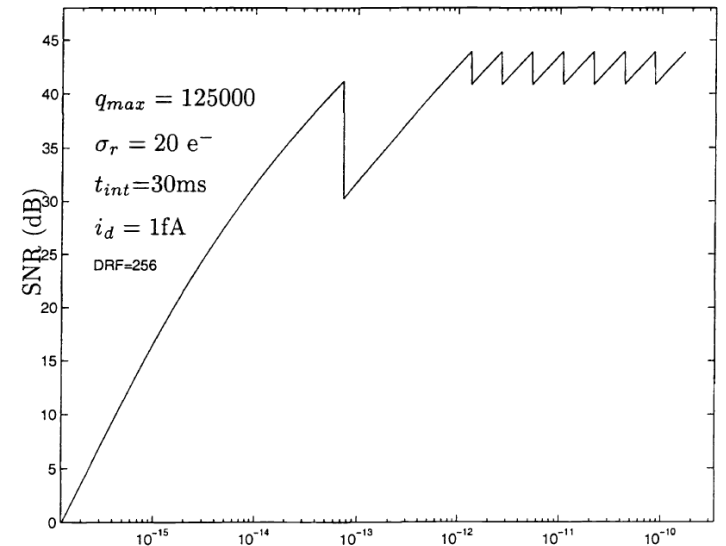
SNR DIP of Multiple Exposure



$$SNR1 = 20 \log \frac{I_{ph} T_l}{\sqrt{I_{ph} T_l}}, \quad SNR2 = 20 \log \frac{I_{ph} T_s}{\sqrt{I_{ph} T_s}}$$

$$SNR_{dip} = SNR1 - SNR2$$

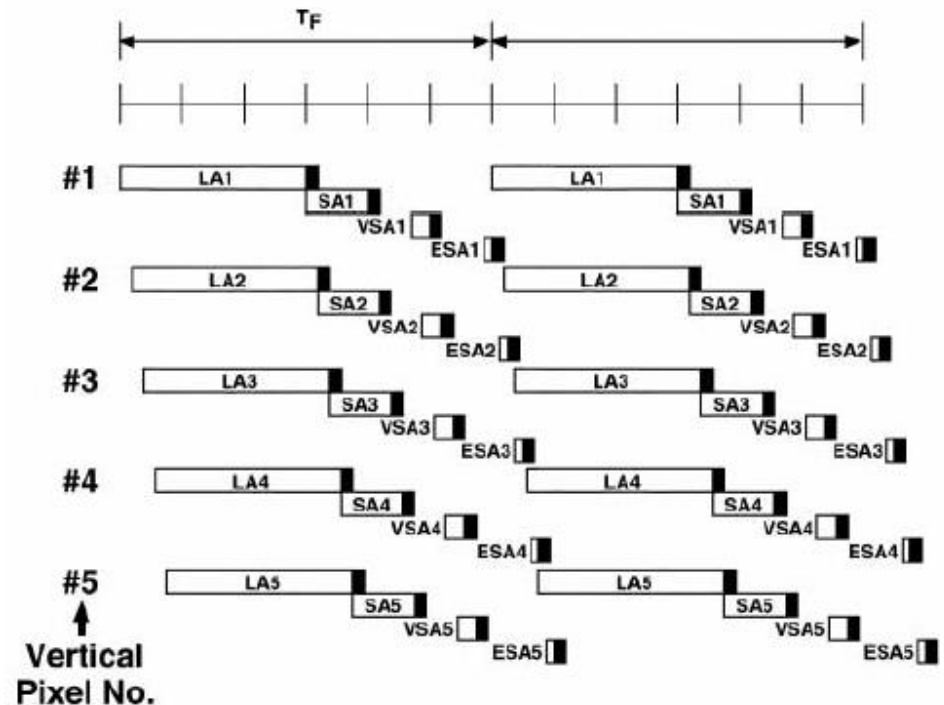
$$= 20 \log \sqrt{\frac{T_l}{T_s}} = 10 \log \frac{T_l}{T_s}$$



Multiple Sampling(cont'd)

- Varying short exposure times
 - $T_{s,min}$ = minimum exposure time.
 - LA: long accumulation
 - SA: short accumulation
 - VSA: very short
 - ESA: extremely short accumulation
- Optimized SNR dip.

$$\Delta DR = 20 \log \frac{T_l}{T_{s,min}}$$



Saturation Detection

- Asynchronized automatic exposure control of each pixel
- Worse reset noise : hard to cancel
- Basic approaches
 - Saturation count
 - Pulse width modulation
 - Pulse frequency modulation

Outline

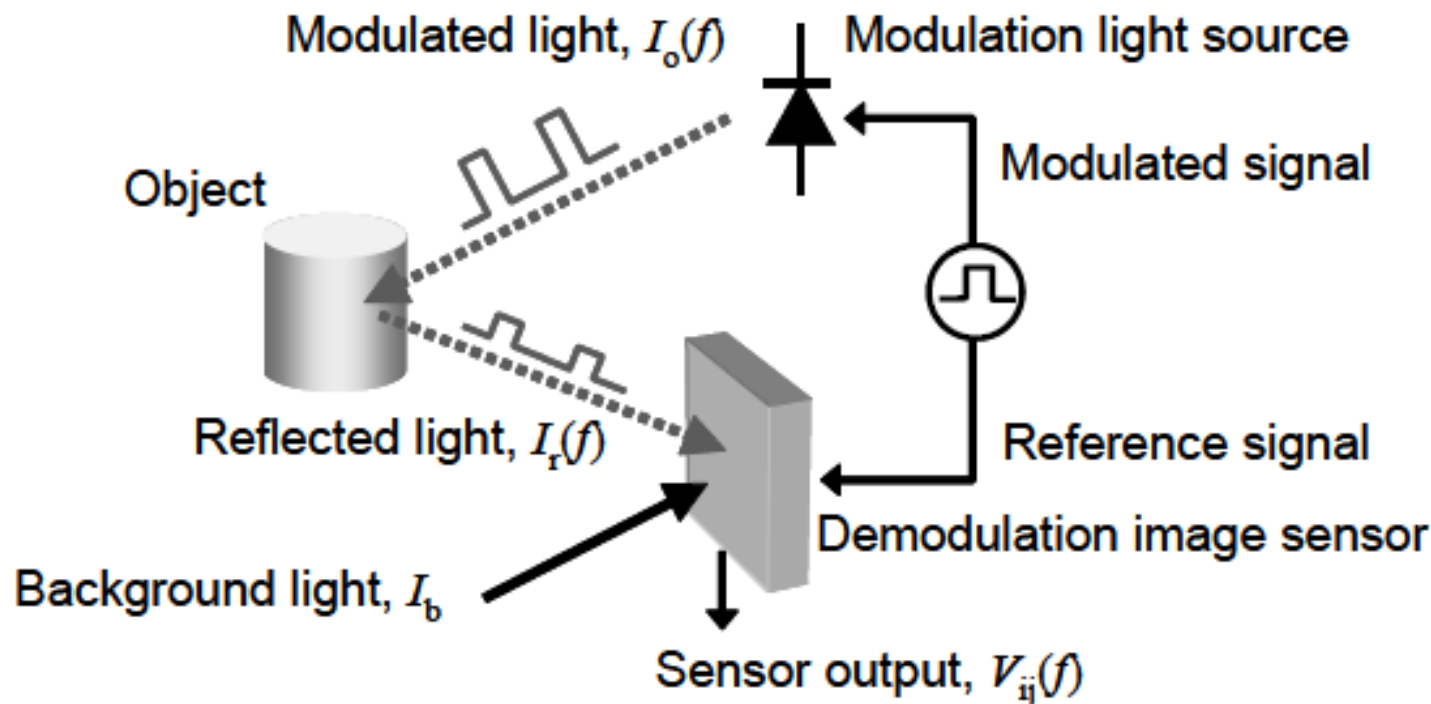
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Demodulation Sensor

- Object illuminated by a modulated light
- Demodulate acquired signal from sensor
- High SNR due to static background removal
- Accumulation will erase the modulation info.
- Applications
 - Intelligent transport system
 - Gesture recognition (xBox)
 - Object tracking
 - 3D range finder (time-of-flight)

Principles of Demodulation

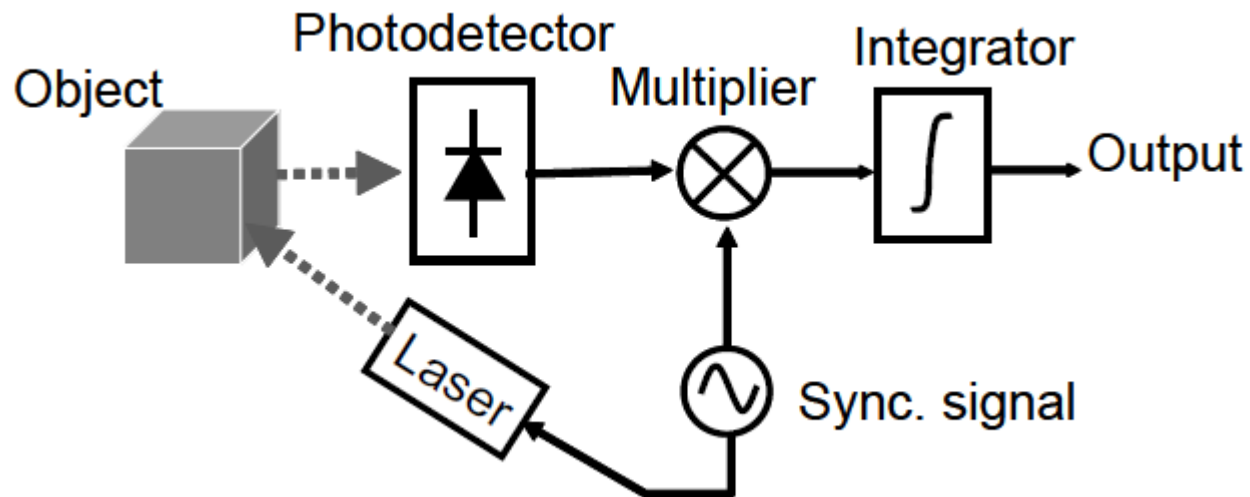
- Concept of a demodulation image sensor



$$V_{out} = \int_{t-T}^t (I_r(\tau) + I_b) m(\tau) d\tau,$$

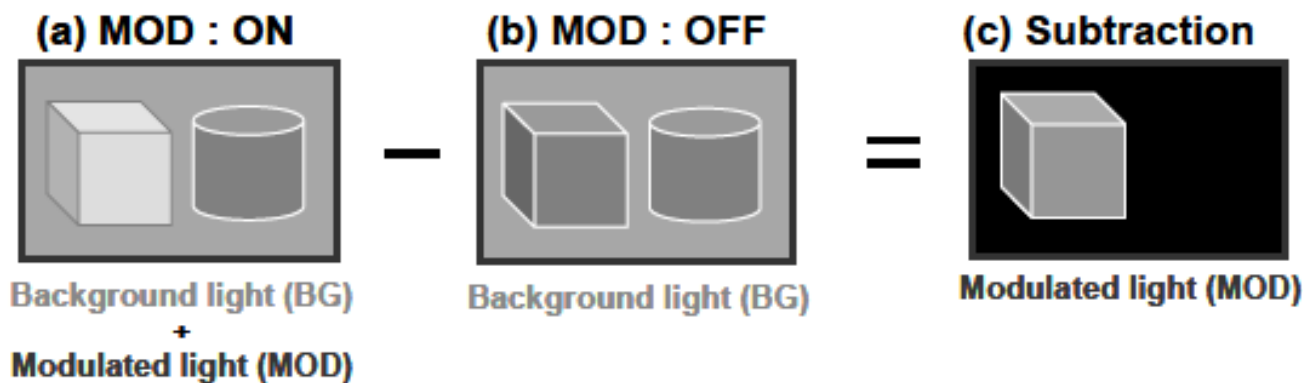
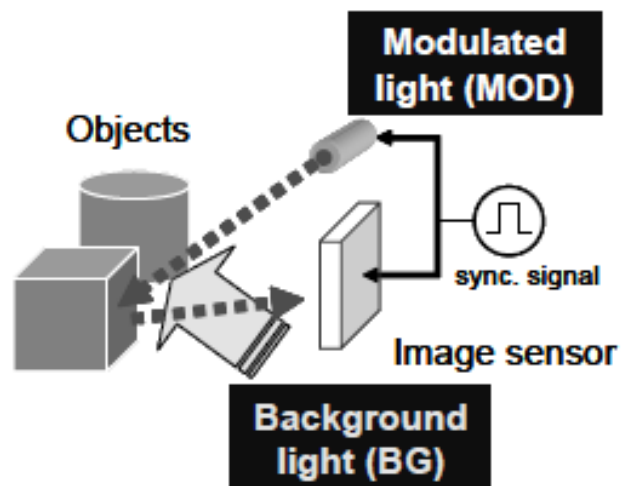
Correlation

- Conceptual illustration of the correlation method



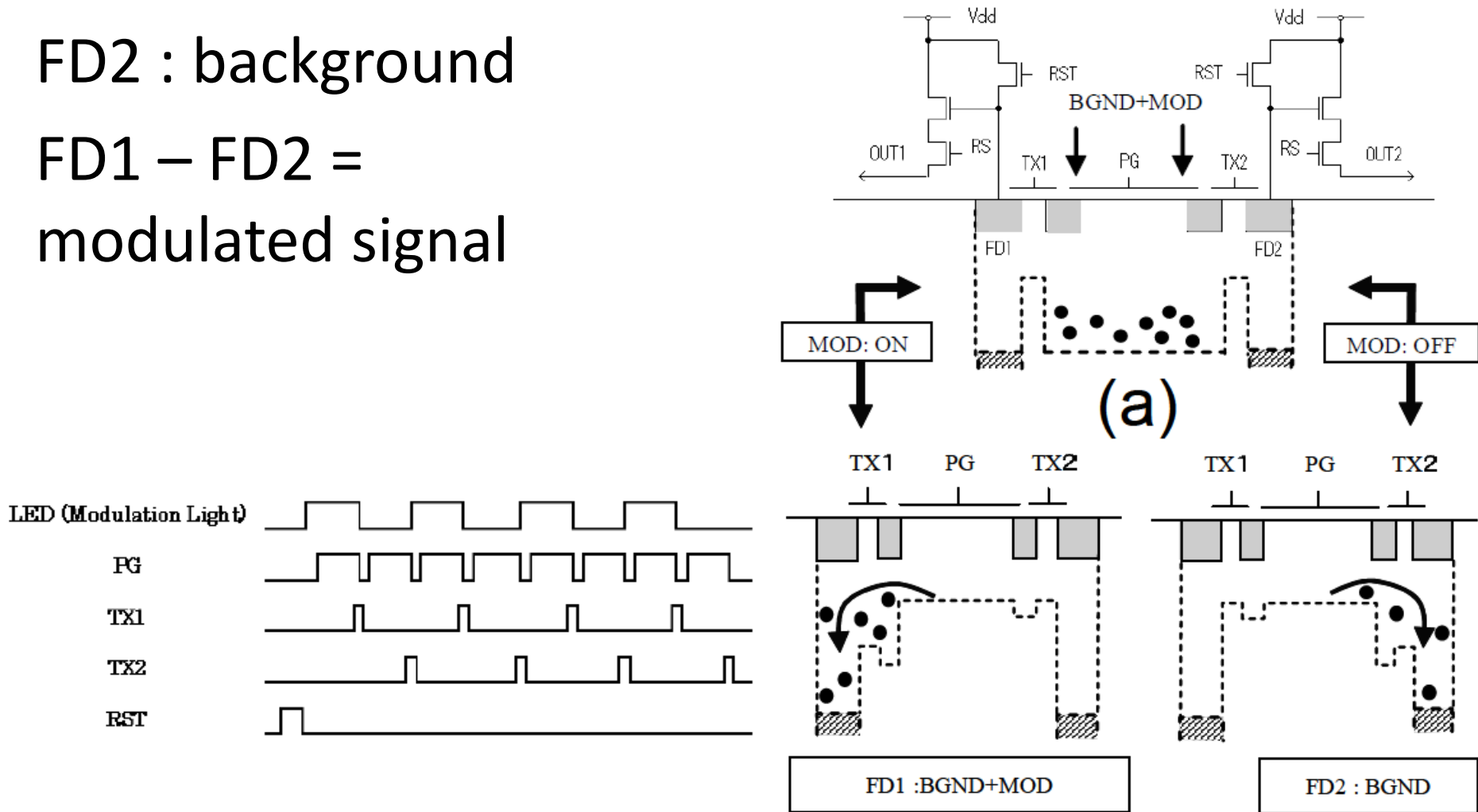
Two Accumulation Regions

- Concept of the two accumulation regions method



Demodulated CIS Pixel

- FD1 : modulation + bgnd
- FD2 : background
- $FD1 - FD2 =$
modulated signal



Sample Image

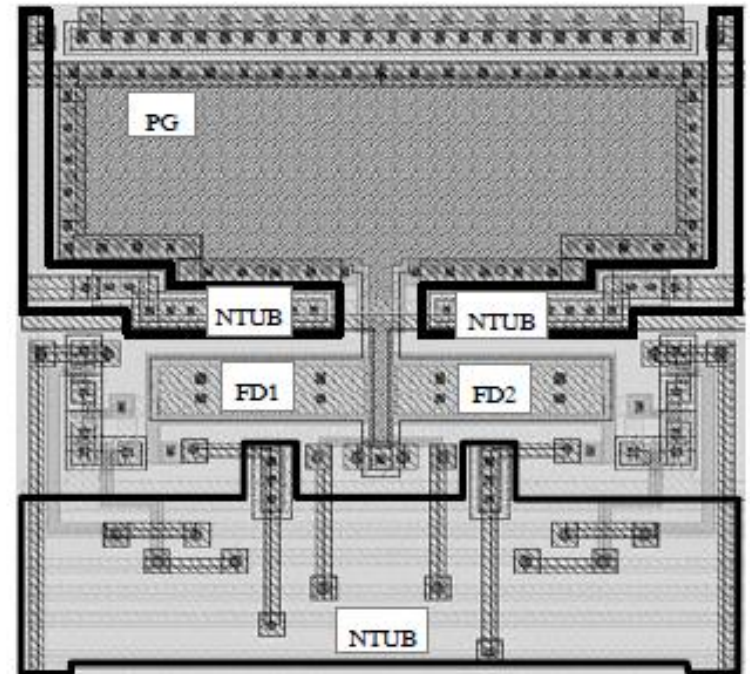
- Cat is illuminated by modulated light only
 - (a) normal image
 - (b) demodulated image



(a)

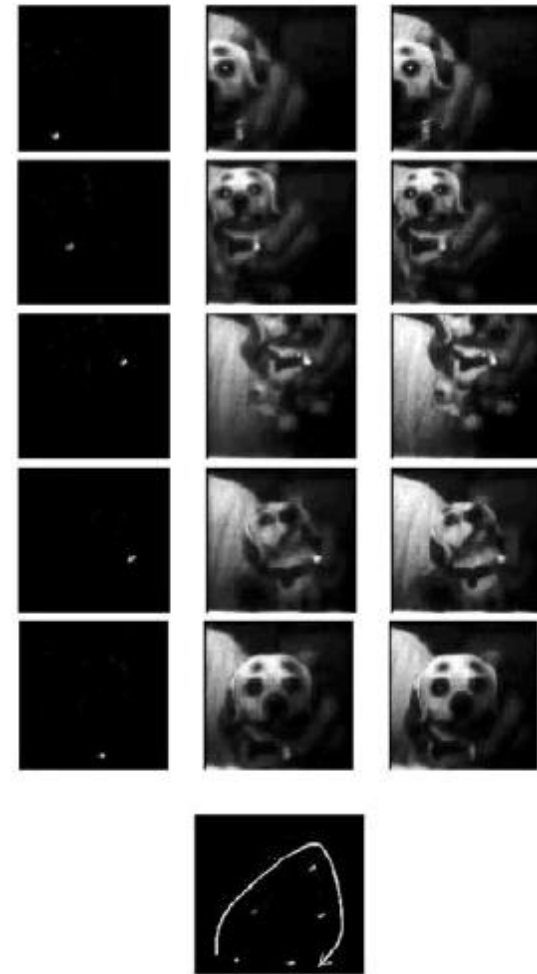


(b)



Tracking

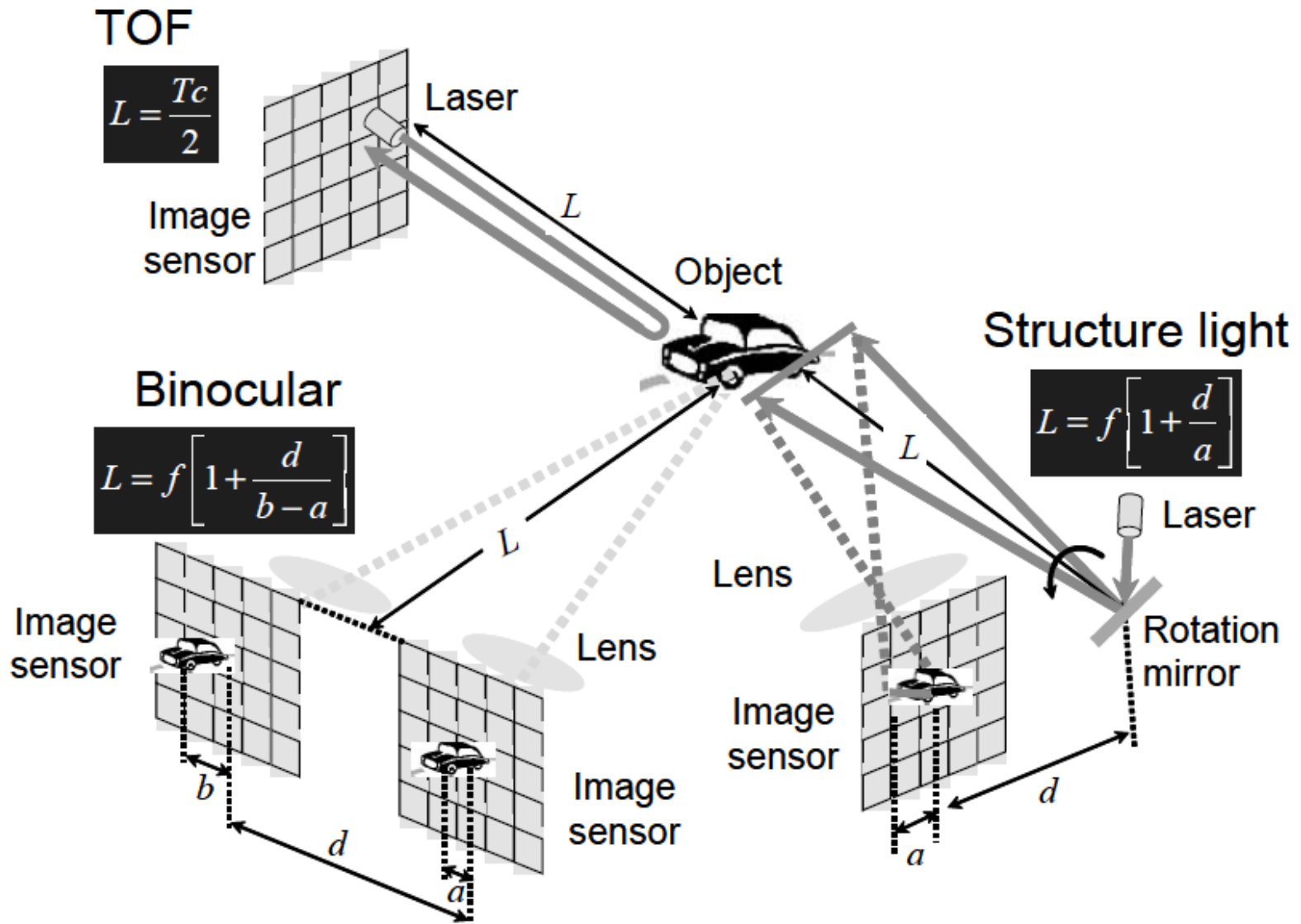
- Demonstration of marker tracking
 - Left column: modulated pattern extracted by the sensor
 - Middle column: modulated and background signal
 - Right column: output from only the background light
 - Bottom figure: the moving trace of the marker



Outline

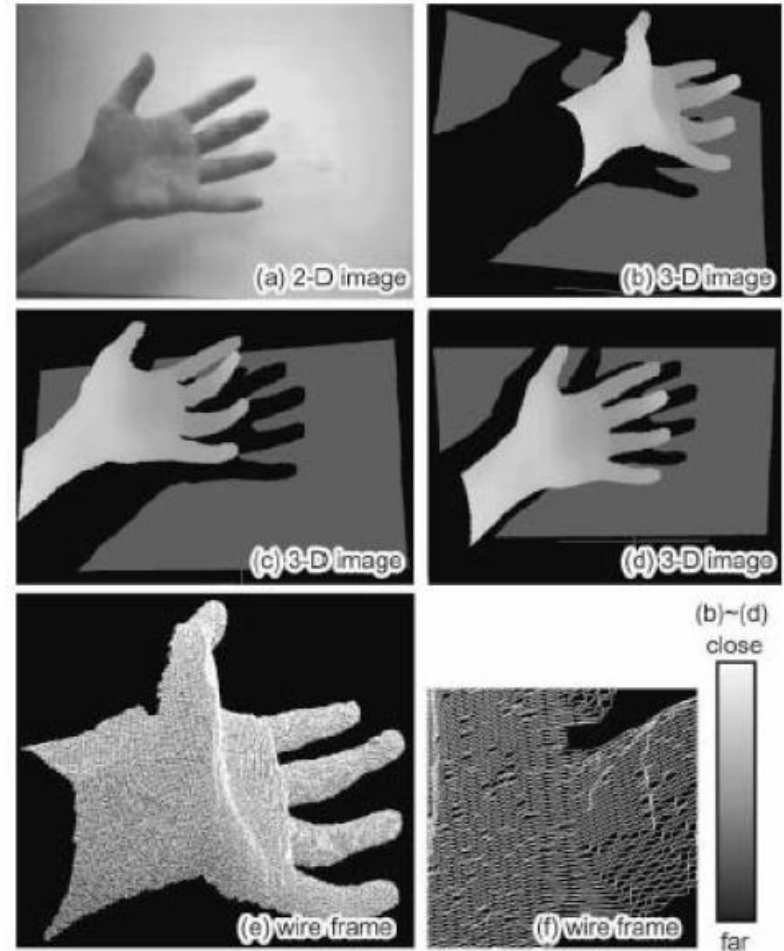
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3D Range Finder



Common 3D Imaging Tech.

- Time-of-flight (TOF)
 - Direct
 - Indirect
- Triangular
 - Binocular
 - Structure light
- Light-intensity



3D Range Finders Methods

Smart CMOS sensors for 3D range finders

Category	Implementation method	Affiliation and Refs.
Direct TOF	APD array	ETH [97, 98], MIT [357]
Indirect TOF	Pulse	ITC-irst [358, 359], Fraunhofer [360, 361], Sizuoka U. [362]
	Sinusoidal	PMD [340, 341, 363, 364], C-SEM [353, 365], Canesta [366], JPL [367]
Triangulation	Binocular	Shizuoka U. [368], Tokyo S-ci. U. [369] Johns Hopkins U. [370, 371]
	Structured light	Carnegie Mellon U. [87, 372] U. Tokyo [350, 356, 373, 374], SONY [157], [375], Osaka EC. U. [342]
Others	Light intensity (Depth of intensity)	Toshiba [376]

Time of Flight (TOF)

- Measure distance by round-trip time of flight
 - L = Distance
 - T = round-trip time
 - C = speed of light
- Simple system

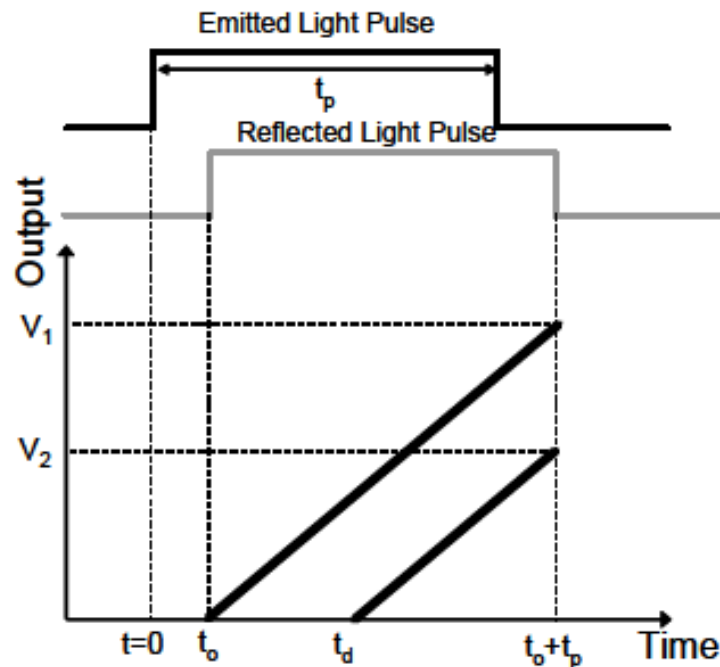
$$L = \frac{Tc}{2},$$

Direct TOF

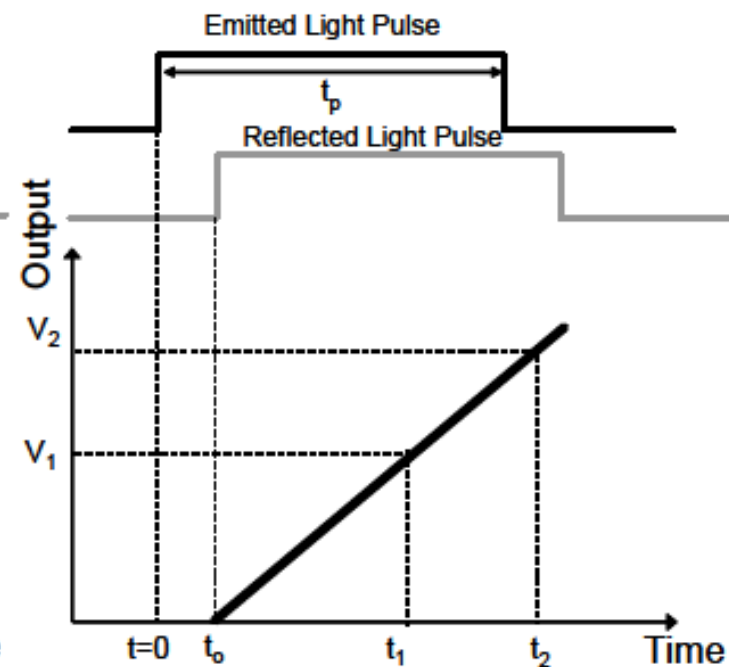
- Measure round-trip time directly
- Require high speed photodetector and high speed precision timing circuit.
 - $L = 3\text{m}$, $T = 10\text{ psec}$
 - Suitable sensor : APD
- Wide measuring distance range : $\text{m} \sim \text{km}$
- Need averaging to improve accuracy

Indirect TOF

- 2 same duration (t_p) pulse with delay t_d
- 2 different duration pulse (t_1 & t_2) with 0 delay

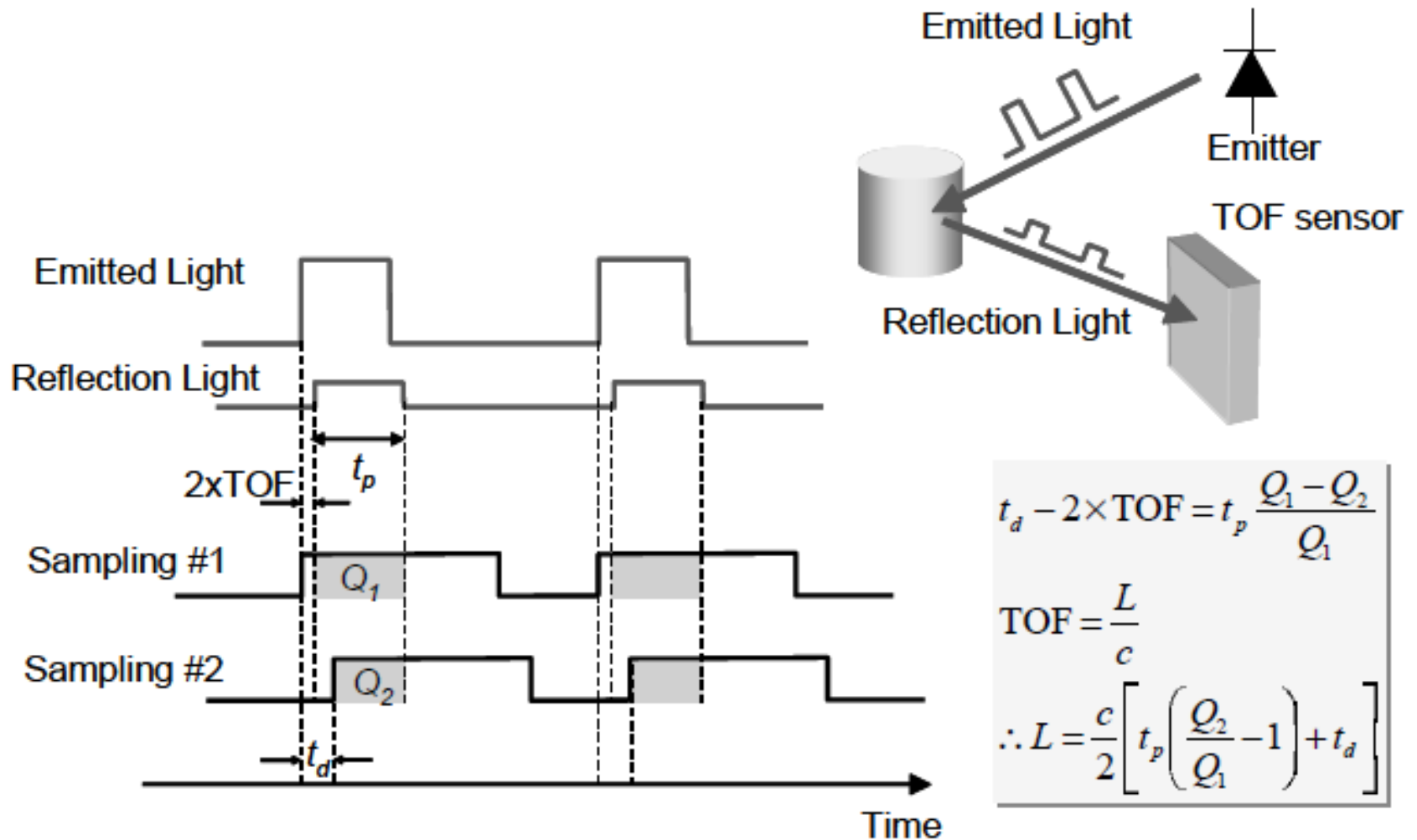


$$L = \frac{c}{2} \left[t_p \left(\frac{V_2}{V_1} - 1 \right) + t_d \right]$$



$$L = \frac{1}{2} c \left(\frac{V_2 t_1 - V_1 t_2}{V_2 - V_1} \right)$$

Indirect TOF with delayed pulses



Indirect TOF(cont'd)

- Operation principle of indirect TOF with sinusoidal emission light

$$A_1 = a \sin \phi + b,$$

$$A_2 = a \sin(\phi + \pi/2) + b,$$

$$A_3 = a \sin(\phi + \pi) + b,$$

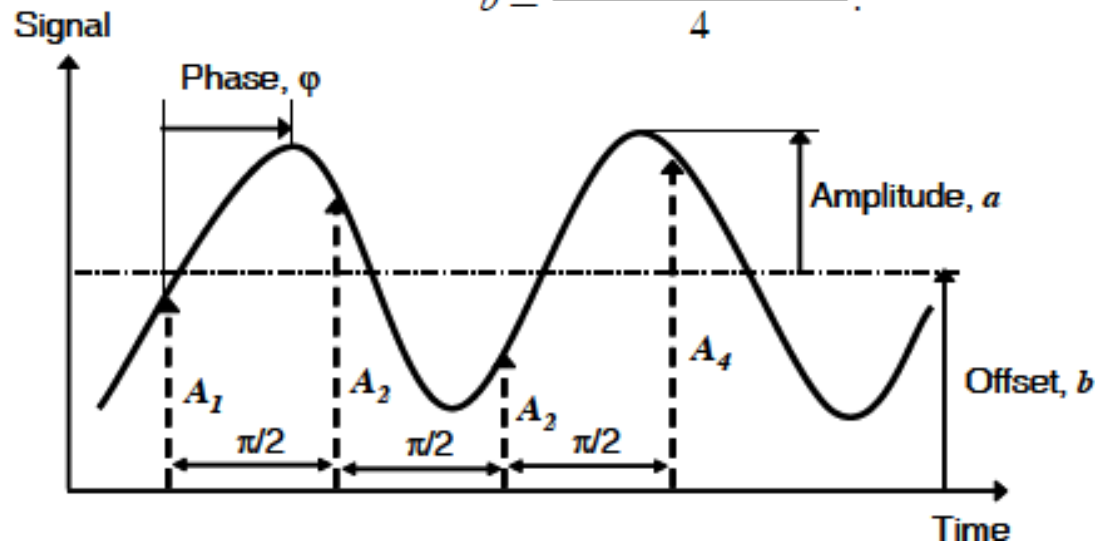
$$A_4 = a \sin(\phi + 3\pi/2) + b.$$

$$\phi = \arctan\left(\frac{A_1 - A_3}{A_2 - A_4}\right).$$

$$a = \frac{\sqrt{(A_1 - A_3)^2 + (A_2 - A_4)^2}}{2}.$$

$$b = \frac{A_1 + A_2 + A_3 + A_4}{4}.$$

$$L = \frac{c\phi}{4\pi f_{mod}},$$



Triangulation

- Measure distance by triangular geometrical arrangement
 - Passive : Binocular (stereo vision) method
 - Active: Structure light method

Binocular Method

- No light source
- Two sensor with identical FOV
 - Complicated system accuracy requirement
- Single sensor with pattern optical-block layer

Structure Light Method

- Require structure light source
 - Require scanning system
 - Require special optics system
- Background cancellation
 - Need to suppress ambient light against the structured light

Depth Key

- Measure distance by focus depth
- Measure distance by reflected intensity
 - Affected by reflectance of the object

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Target tracking

- Object extraction
 - Modulation techniques
 - Structure light
- Centroid finding with frame difference
 - Maximum detection
 - Projection
 - Resistive network
 - Digital processing

Target Tracking Summary

Smart CMOS sensors for target tracking							
Method	Preprocess	Tech. (μm)	Pixel #	Pixel size (μm)	Speed	Power consum.	Ref.
MaxDet.	WTA & 1D-RN	2	24×24	62×62	7 kpix/s		[383]
MaxDet.	1D-RN & comparator	0.6	11×11	190×210	$50 \mu\text{s}$ (sim.)		[384]
Projection	Current sum	2	256×256	35×26	10 ms		[173]
Projection	Edge detect	2	Fovea 9×9 , periphery 19×17	Fovea 150×150 , periphery 300×300	10 lpix/s	15 mW	[385]
Projection	Binarization	0.18	80×80	12×12	1000 fps	30 mW	[386]
Projection	Charge sum	0.6	512×512	20×20	1620 fps	75 mW	[387]
2D-RN		0.25	100×100 (hex.)	87×75.34	$\sim 7 \mu\text{s}$	36.3 mW	[45]
CNN		0.18	48×48	85×85	$500 \mu\text{s}$, ~ 725 MIP-S/mW	243 μW	[388]
Digital process.	ADC	0.5	64×64	80×80	1 kHz	112 mW	[61]

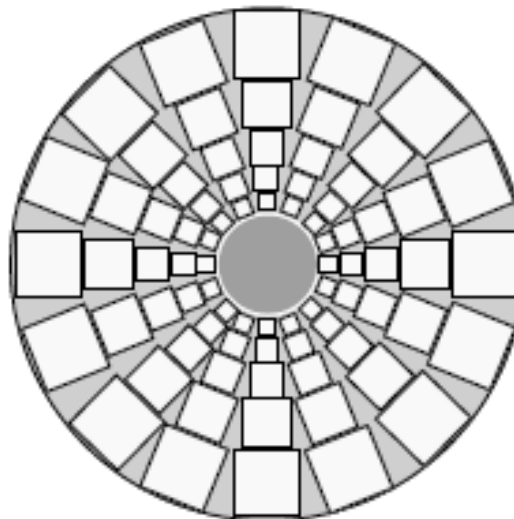
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Non-orthogonal Arrangement

- Pixel arrangement of a foveate image sensor
 - the pixel size increases by square root
 - the pixel pitch logarithmically decreases
 - the circle area of the center shows the control circuits

$$r = \sqrt{x^2 + y^2}$$
$$\theta = \arctan\left(\frac{y}{x}\right).$$

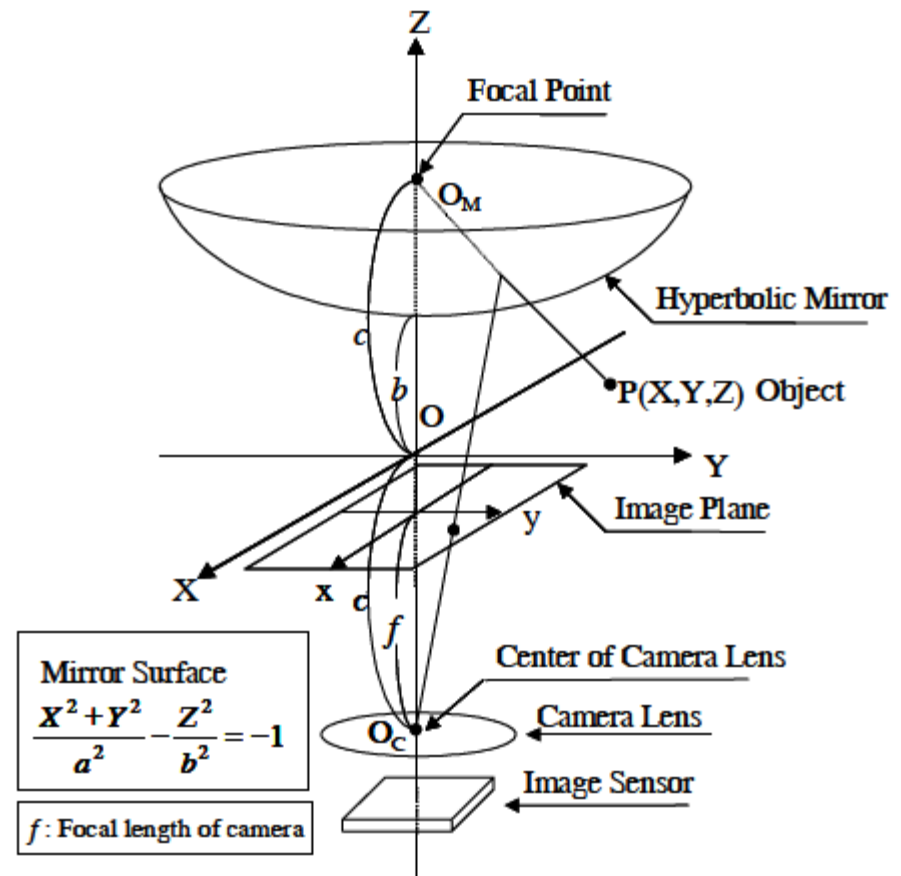
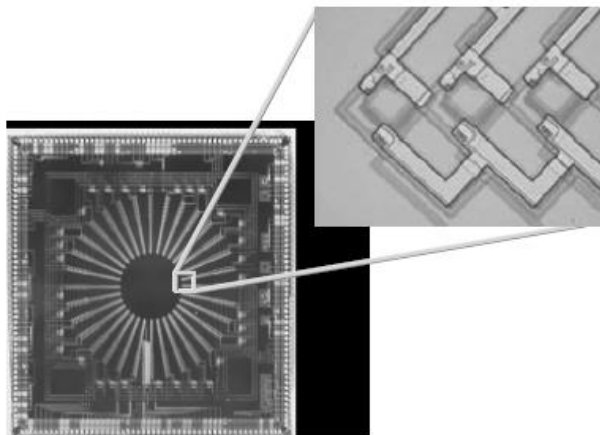


Non-orthogonal Arrangement

- Configuration of a Hyper omni vision (HOVI) system

$$x = \frac{Xf(b^2 - c^2)}{(b^2 + c^2)Z - 2bd\sqrt{X^2 + Y^2 + Z^2}},$$

$$y = \frac{Yf(b^2 - c^2)}{(b^2 + c^2)Z - 2bd\sqrt{X^2 + Y^2 + Z^2}}.$$



Non-orthogonal Arrangement(cont'd)

- HOVI's images (a Japanese character)
 - (a) output of conventional HOVI system
 - (b) output of foveate sensor



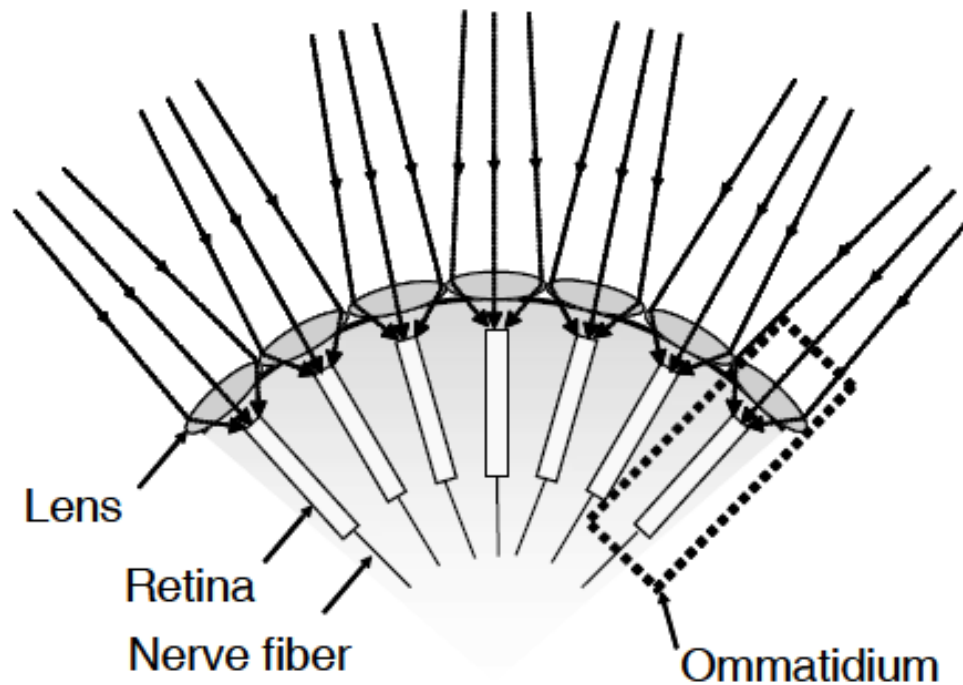
(a)



(b)

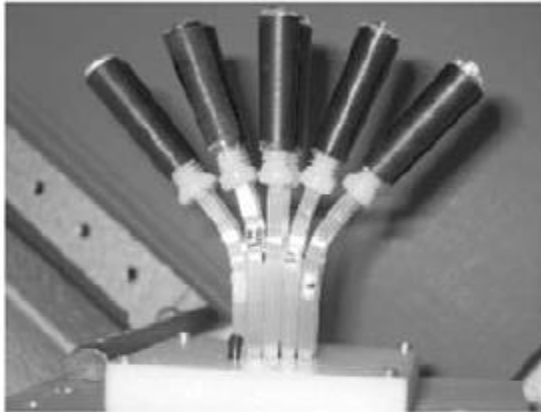
Dedicated Optics

- Concept of an apposition compound eye system



Dedicated Optics(cont'd)

- Photographs of the prototype of DragonflEye
 - (a) close up of eyelet bundle
 - (b) total system

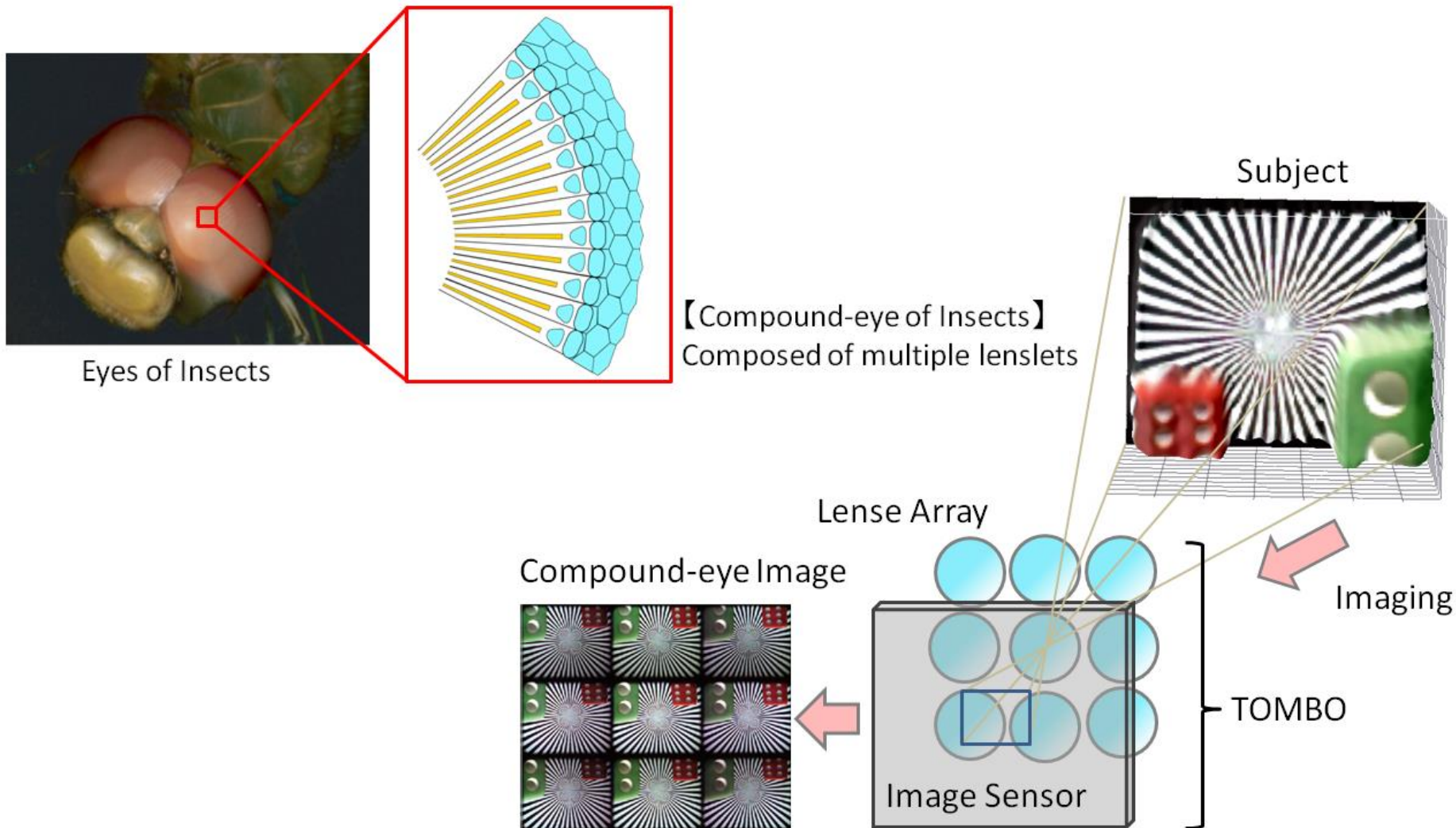


(a)



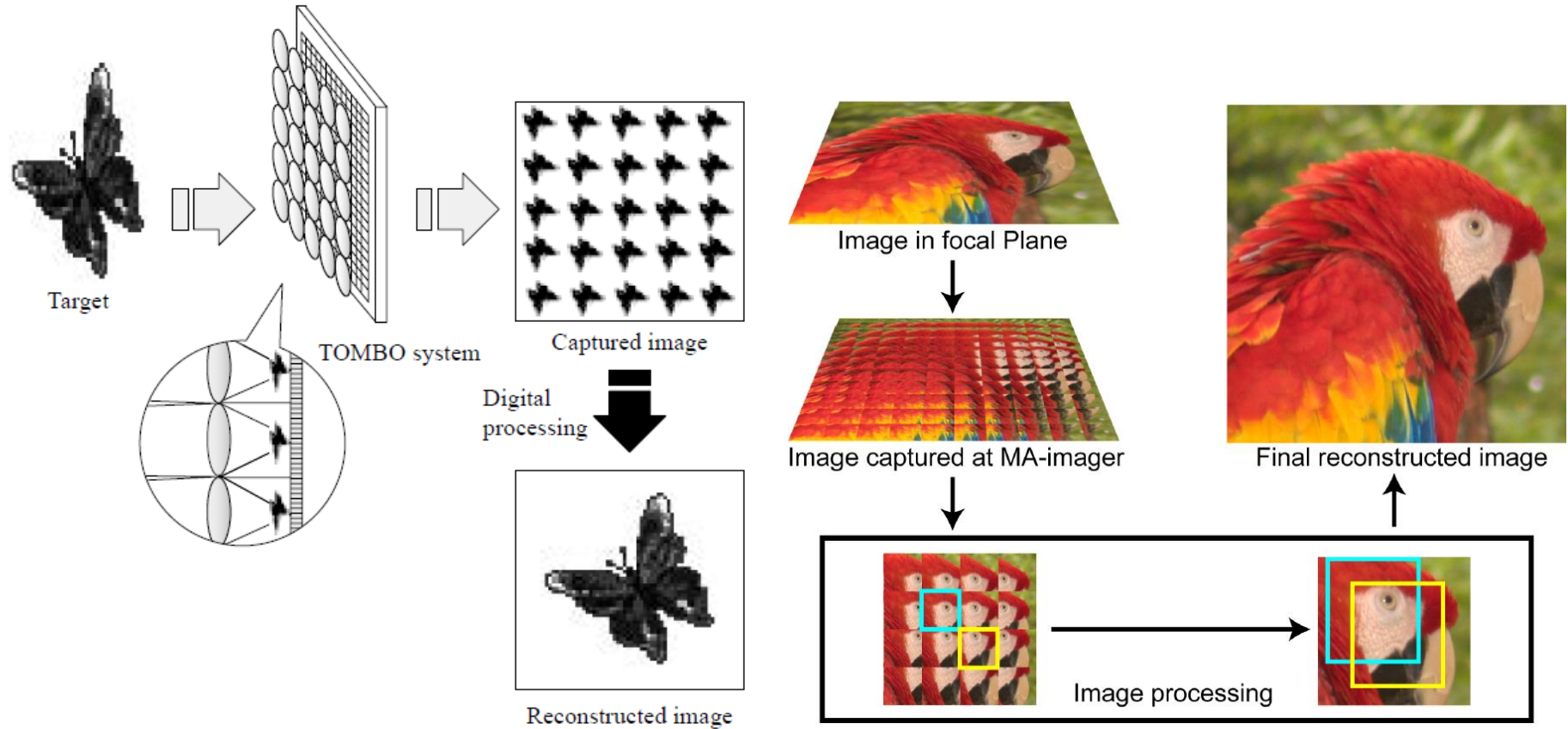
(b)

Compound Eye

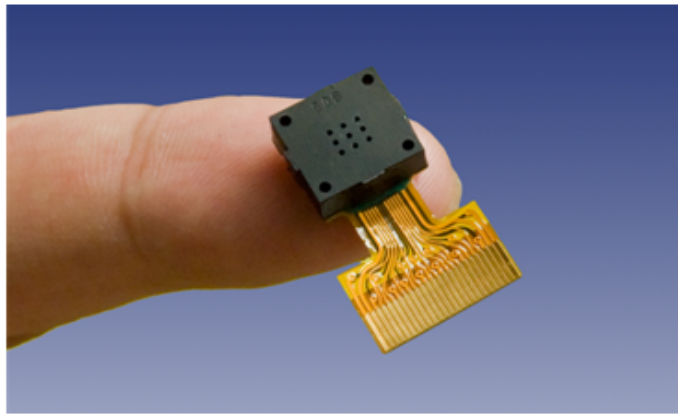


Dedicated optics(cont'd)

- Concept of TOMBO system

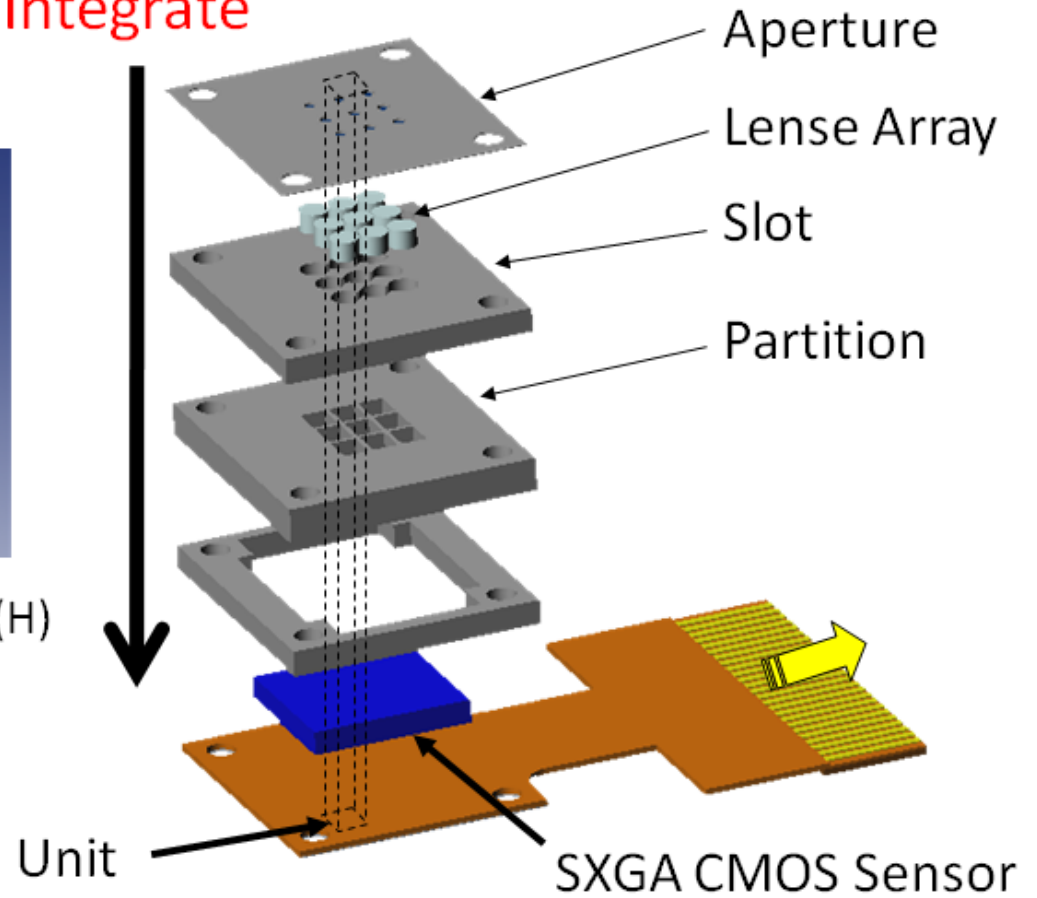


Structure of TOMBO

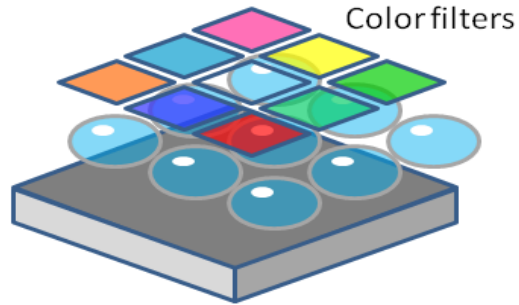


9.6mm(W) × 9.0mm(D) × 3.4mm(H)

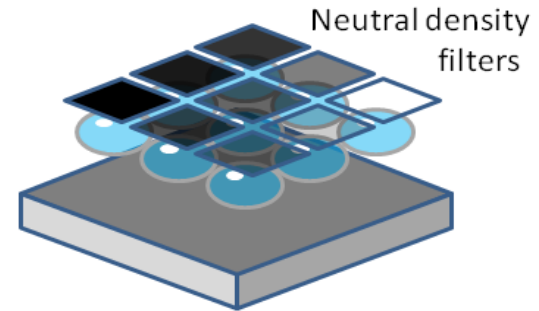
Integrate



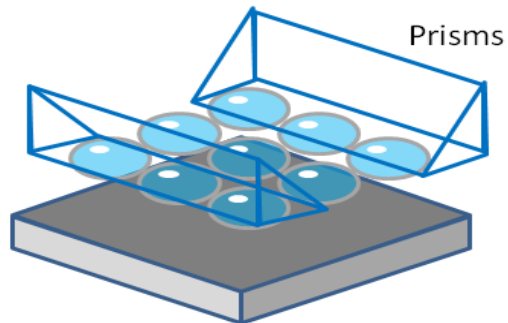
Functional Imager of TOMBO



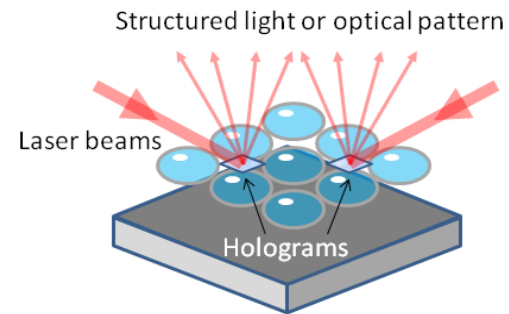
Multi-spectral imaging



High dynamic-range imaging



Wide field-of-view imaging



Integration of micro projectors

Re-Focusing

