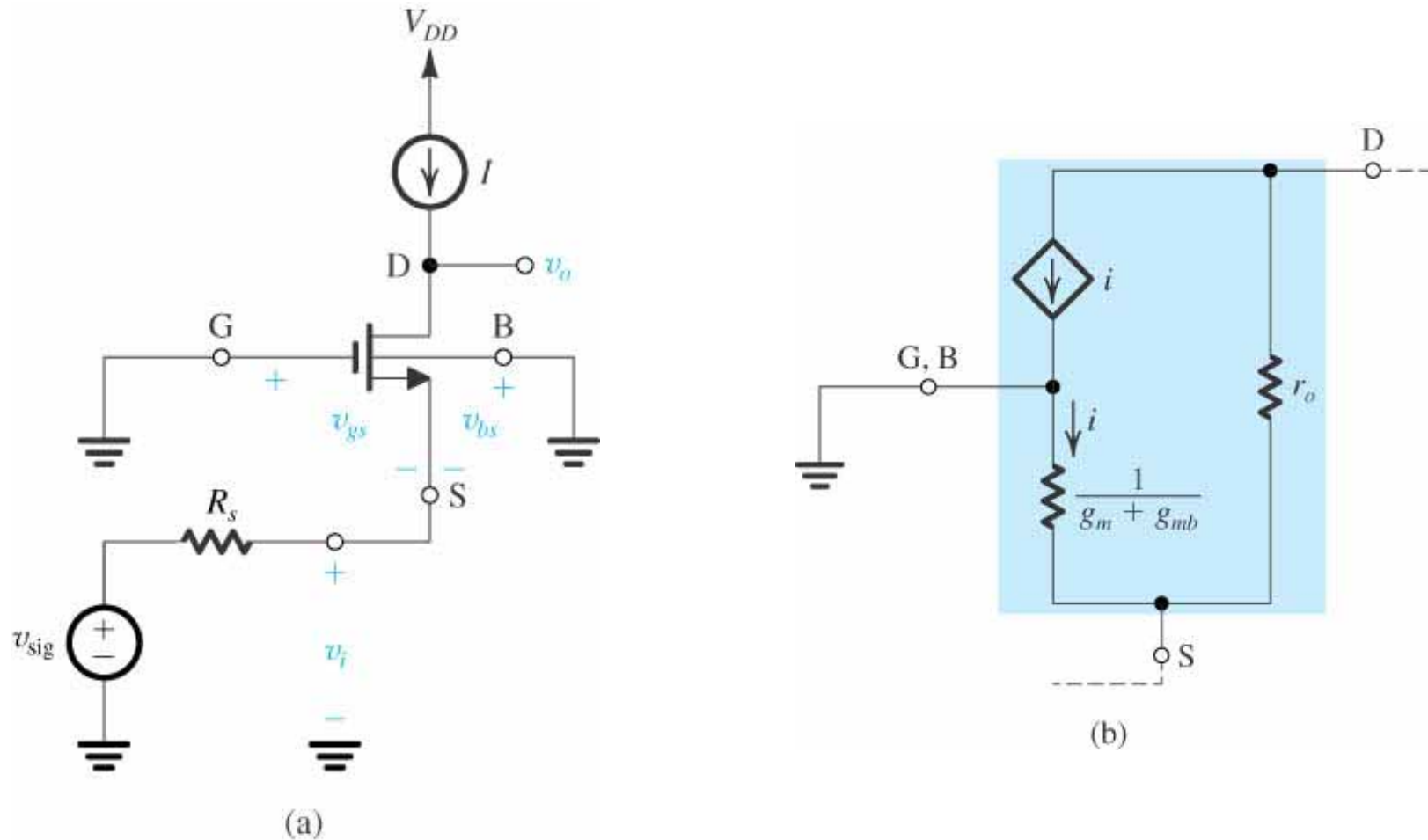


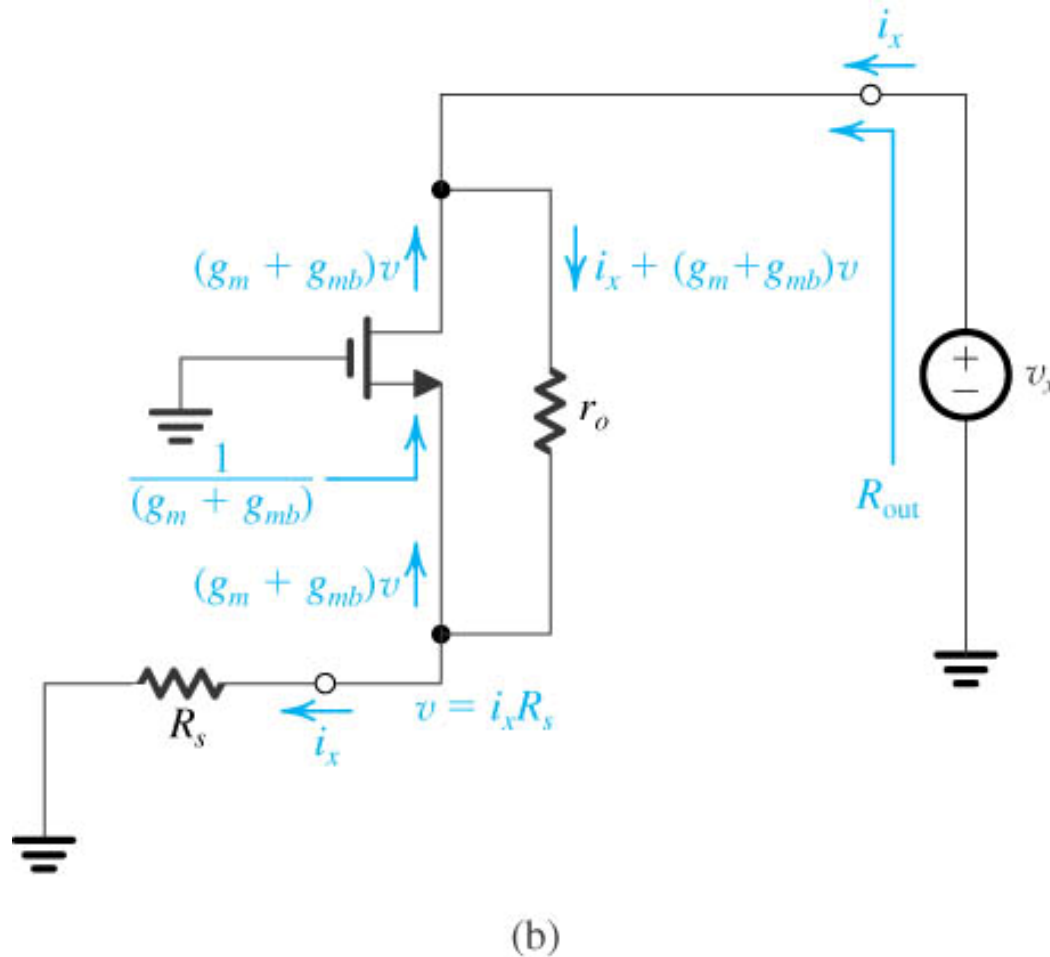
Outline

- Comparison between the MOS and the BJT
- From **discrete** circuit to **integrated** circuit
 - Philosophy, Biasing, ...etc.
- Frequency response
- The **Common-Source** and **Common-Emitter** amplifier with active loads
- The **Common-Gate** and **Common-Base** amplifier with active load
- The **Source** and **Emitter Follower**
- The CS and CE amplifier with **source degeneration**
- Current mirrors with improved performance
- **Cascode** amplifier and **transistor pairings**

6-5 Common-Gate and Common-Base amplifiers with active loads



Low-frequency characteristics of the CG amplifier

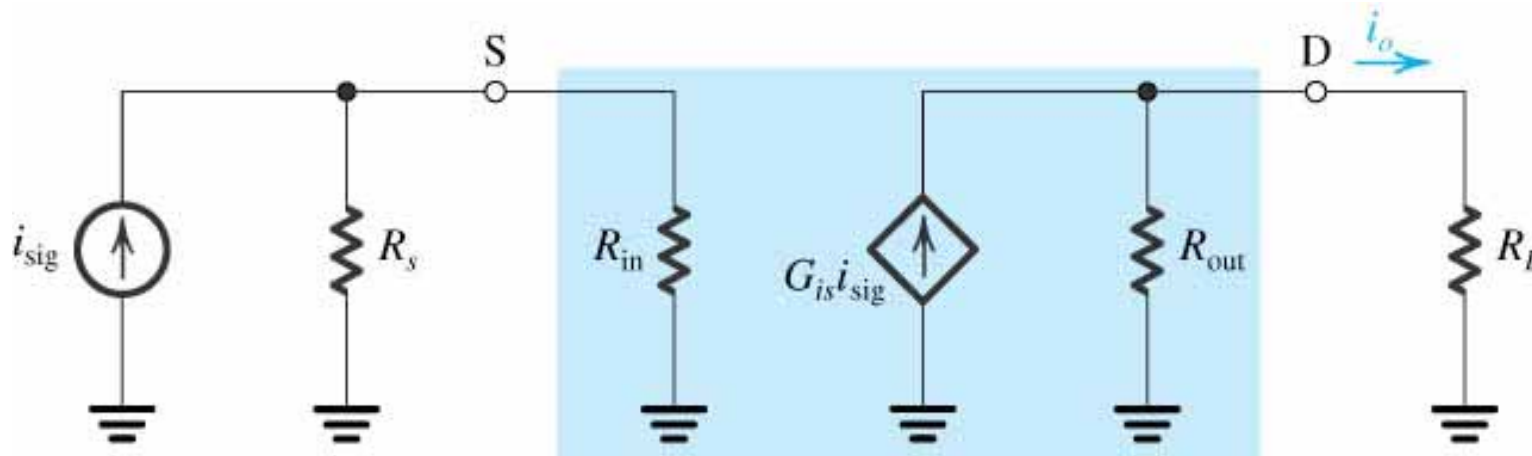


$$R_{out} = r_o + [1 + (g_m + g_{mb})r_o]R_s$$

Since $g_m \cong 10g_{mb}$

$$R_{out} \cong r_o + (1 + g_m r_o)R_s$$

CG amplifier can be used as a current buffer

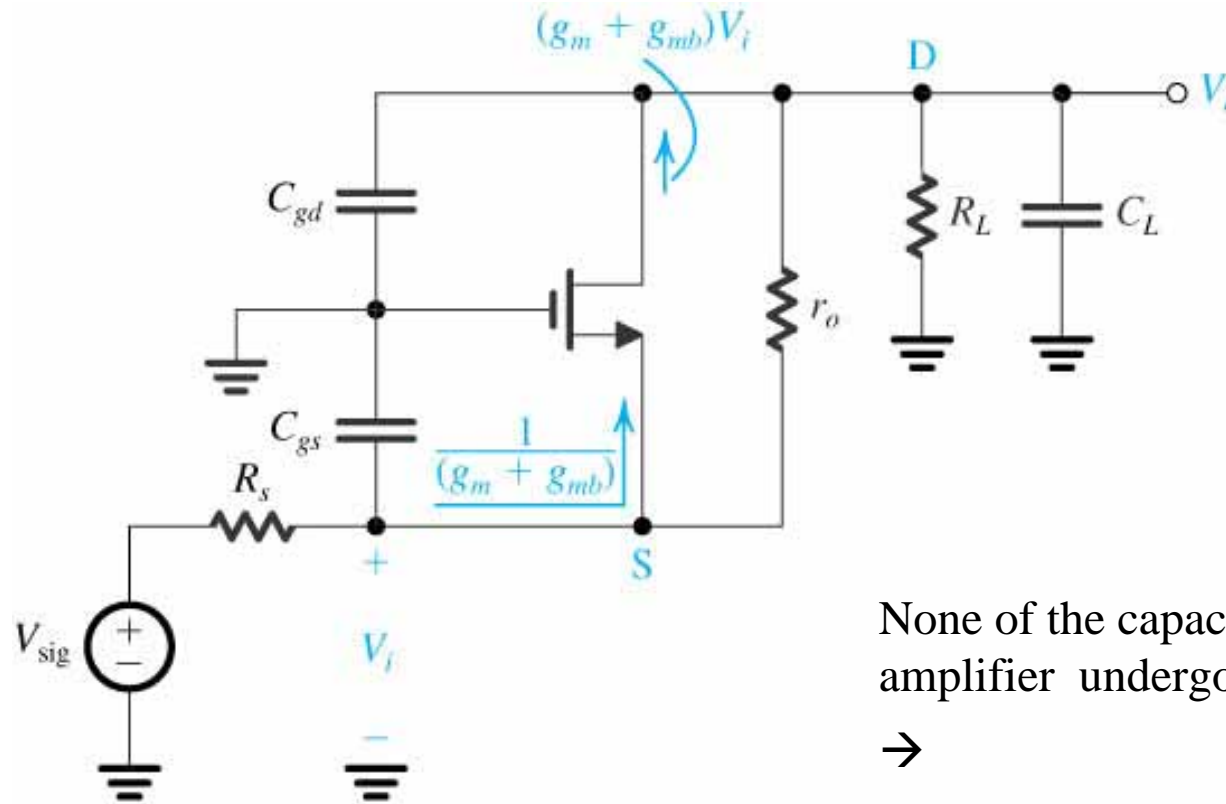


$$R_{in} \cong \frac{1}{g_m + g_{mb}} + \frac{R_L}{A_{vo}}$$

$$R_{out} \cong r_o + (1 + g_m r_o) R_s$$

$$G_{is} = A_{vo} \frac{R_s}{R_{out}} \cong 1$$

High-frequency response of a CG amplifier

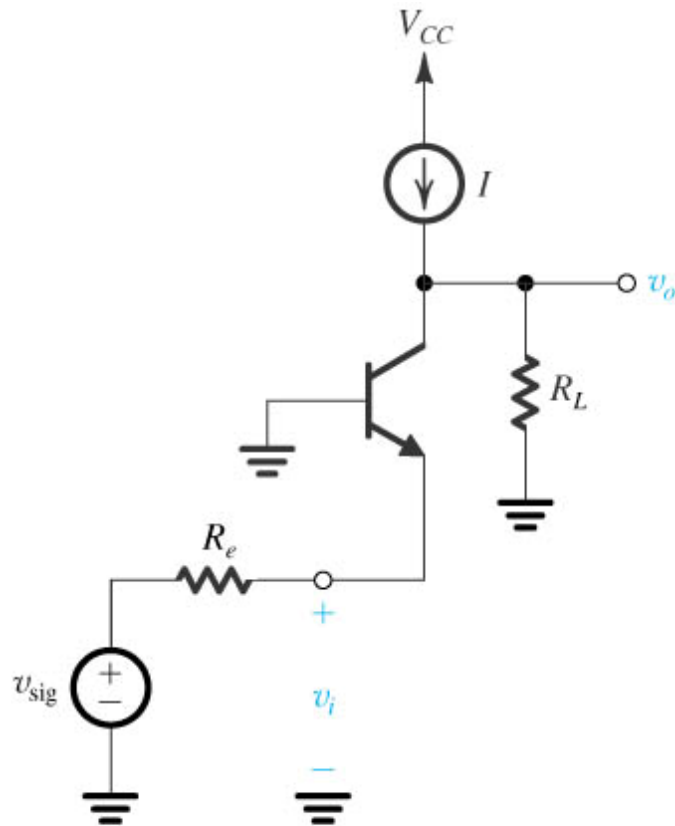


(a)

None of the capacitors in the CG amplifier undergoes the Miller effect



Common-Base amplifier



$$R_{in} \cong r_e + \frac{R_L}{A_o}$$

$$R_{out} \cong (1 + g_m R'_e) r_o$$

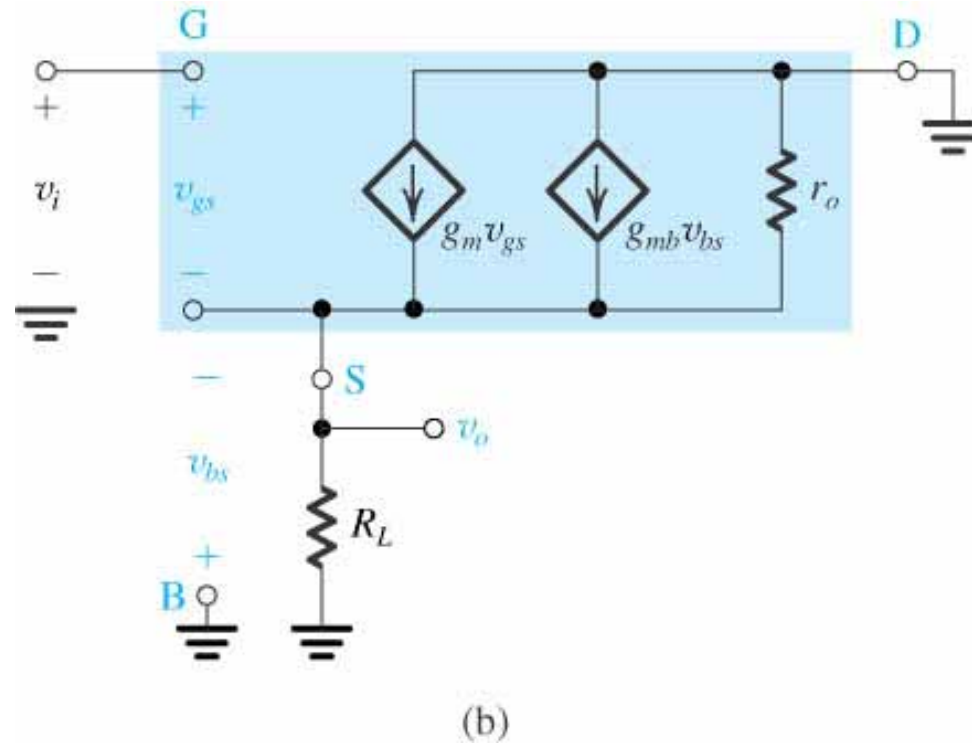
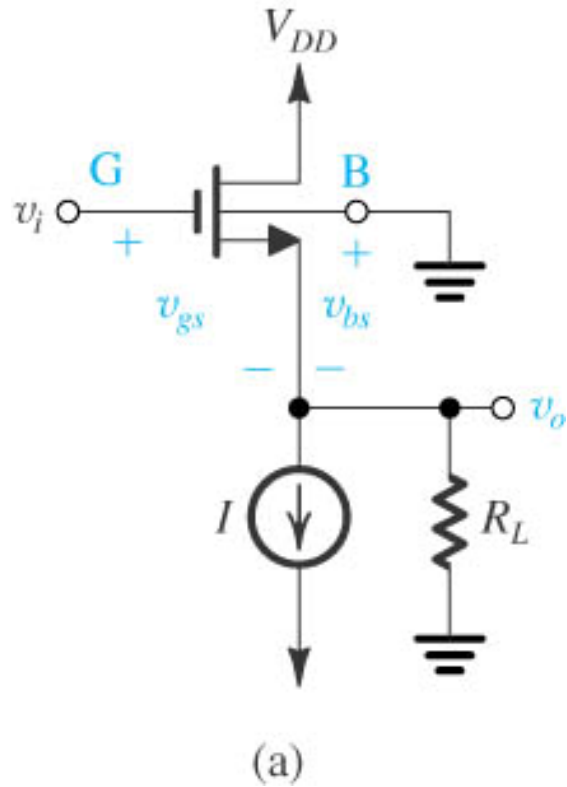
where $R'_e \cong r_\pi \parallel R_e$

(a)

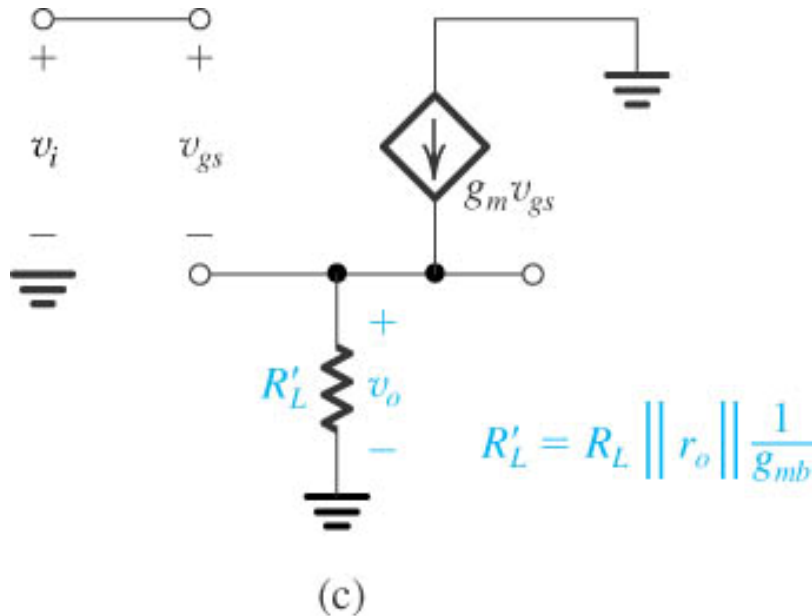
Outline

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6-6 The Source- and Emitter-follower



Low-frequency characteristics of a Source follower



$$R_{in} = \infty$$

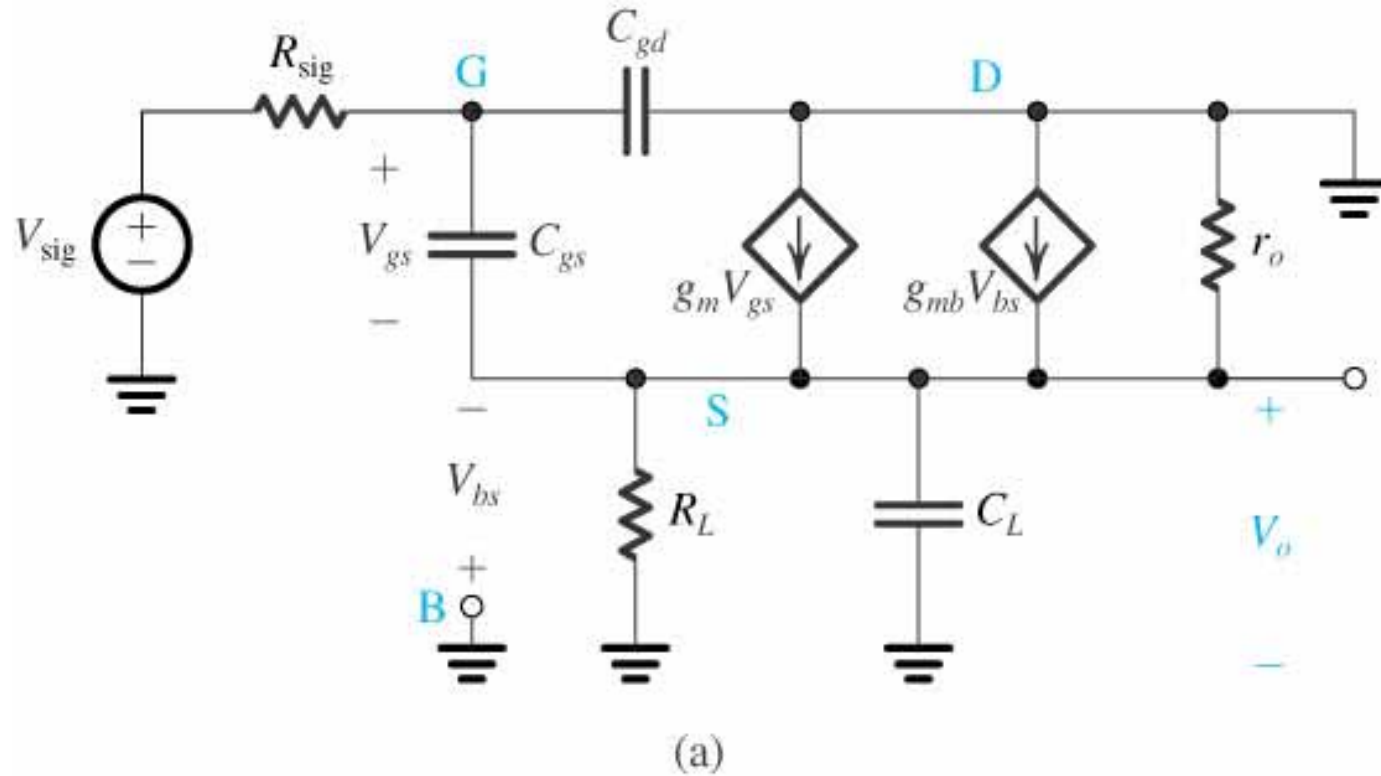
$$R_{out} = \frac{1}{g_m} \parallel \frac{1}{g_{mb}} \parallel r_o$$

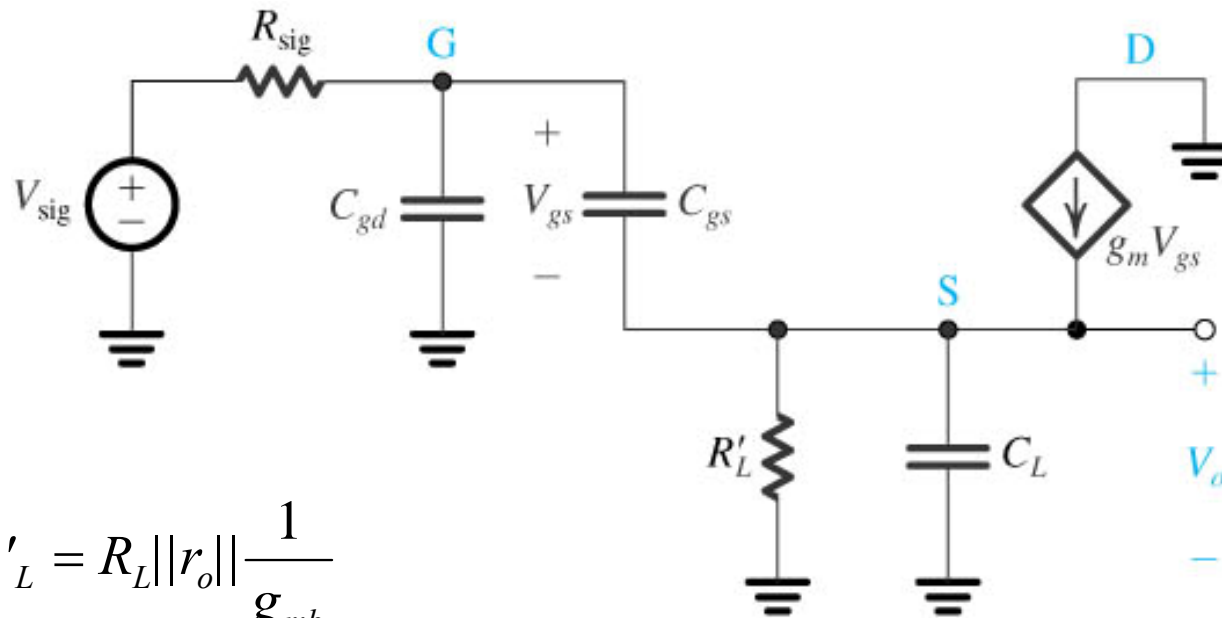
$$A_{vo} = \frac{g_m R'_L}{1 + g_m R'_L} \Bigg|_{R_L = \infty} = \frac{g_m r_o}{1 + (g_m + g_{mb}) r_o}$$

$$\Rightarrow A_{vo} \cong \frac{g_m}{g_m + g_{mb}} = \frac{1}{1 + \chi}$$

\Rightarrow CD amplifier can function as a voltage buffer!!

High-frequency response of a Source Follower





$$R'_L = R_L || r_o || \frac{1}{g_{mb}}$$

(b)

Zeros:

$$s_Z = -\frac{g_m}{C_{gs}}$$

Dominant pole:

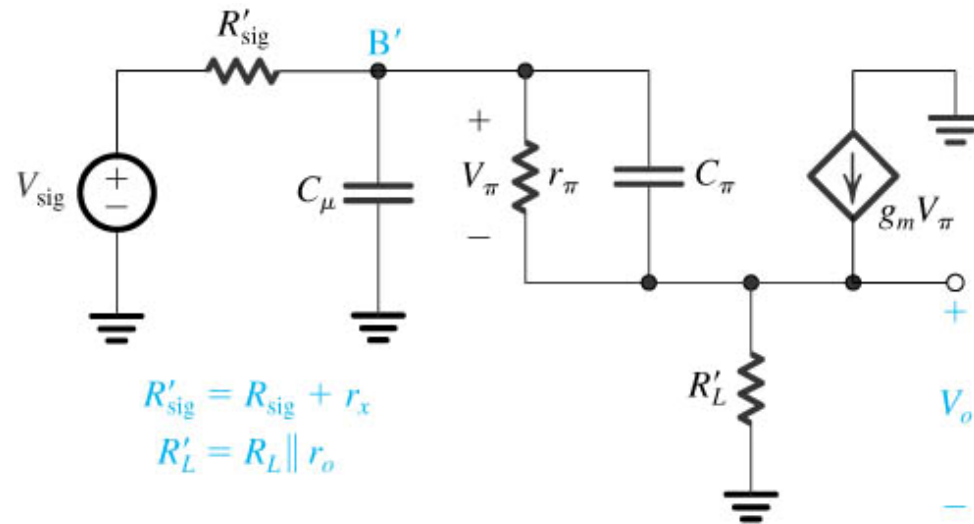
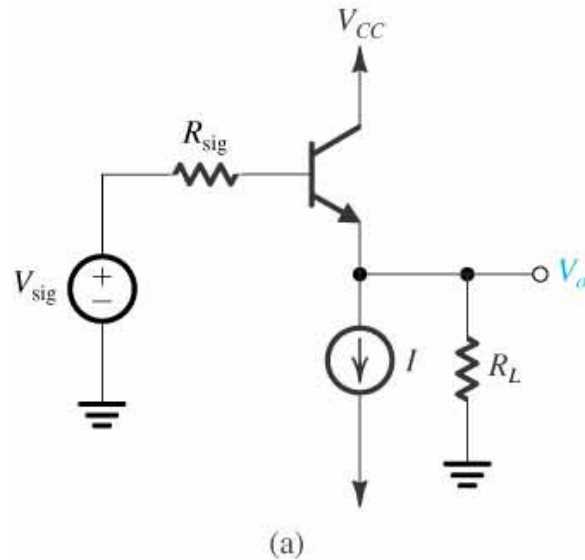
$$R_{gd} = R_{sig}$$

$$R_{CL} = R'_L || \frac{1}{g_m}$$

$$R_{gs} = \frac{R_{sig} + R'_L}{1 + g_m R'_L}$$

$$f_H = 1/2\pi(C_{gd}R_{sig} + C_{gs}R_{gs} + C_L R_{CL})$$

The Emitter Follower



$$R'_{sig} = R_{sig} + r_x$$

$$R'_L = R_L \parallel r_o$$

$$s_z = -\frac{1}{C_\pi r_e}$$

$$R_\mu = R'_{sig} \parallel [r_\pi + (\beta + 1)R'_L]$$

$$R_\pi = \frac{R'_{sig} + R'_L}{1 + \frac{R'_{sig}}{r_\pi} + \frac{R'_L}{r_e}}$$

$$f_H = 1/2\pi(C_\mu R_\mu + C_\pi R_\pi)$$

Summary – the intuition for various single-stage amplifiers

